

(Langzeit-) Stabilität von SOFC-Komponenten

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Basic Concepts in Reliability Engineering

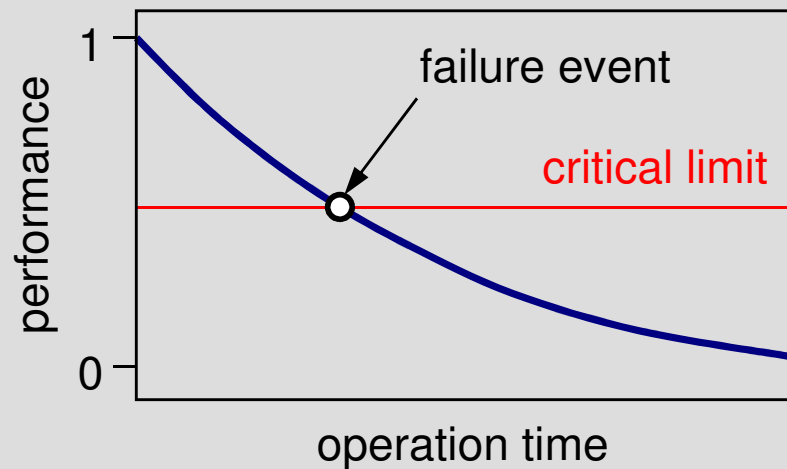
Definition of Failure Event and Time-To-Failure

soft failure

gradual performance loss until (pre-defined) critical level is reached.

example

- voltage/ power degradation in fuel cells



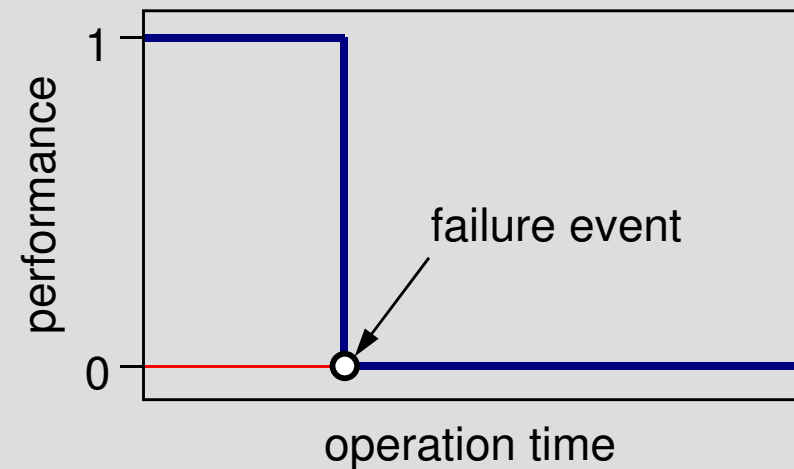
(Meeker et al., Technometrics, 40, 1998)

hard failure

sudden loss of functionality – the device stops working.

example

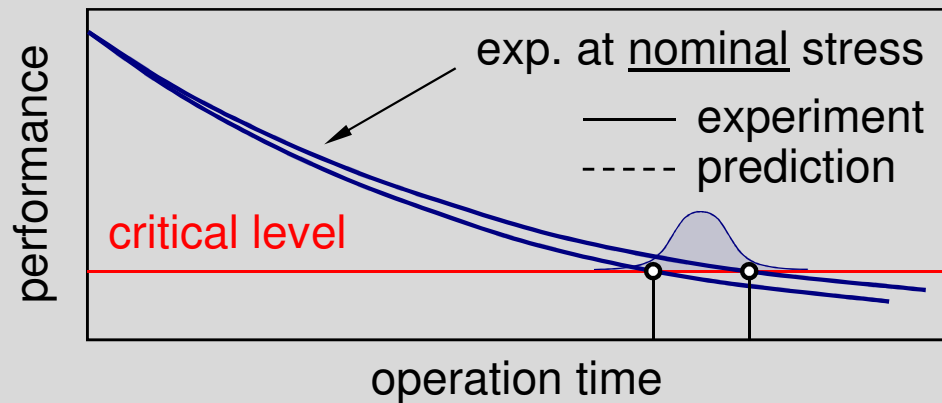
- light bulb burns out



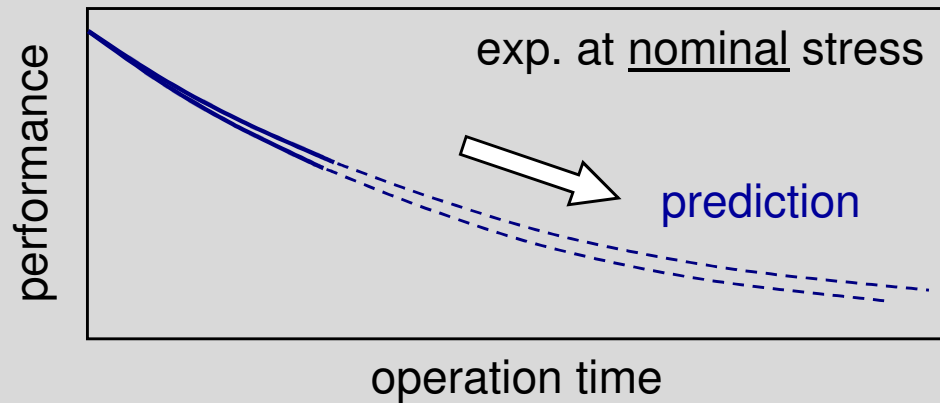
Lifetime and Degradation Assessment

Overview of Life Testing Methods

"conventional" life testing

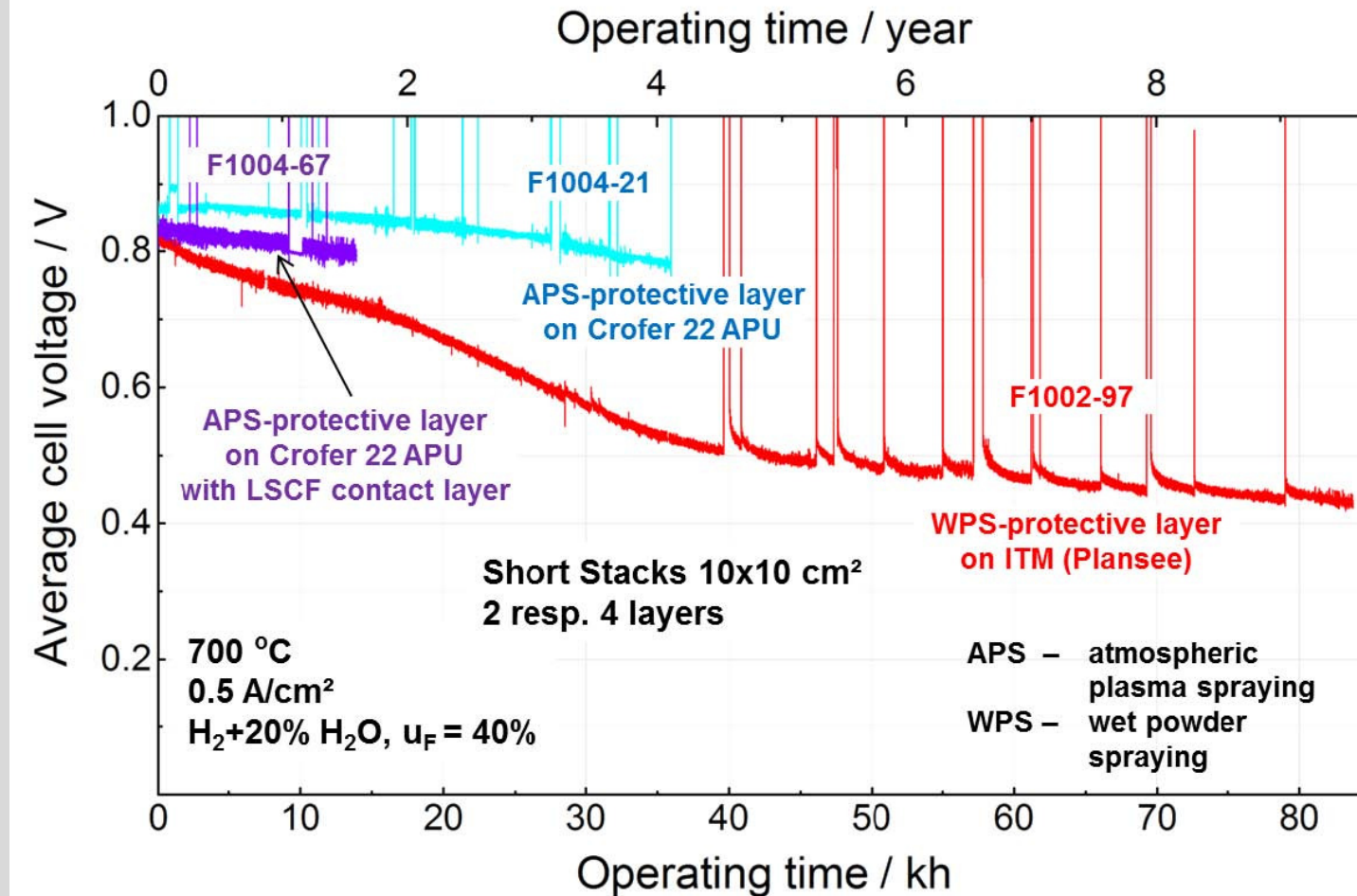


degradation testing

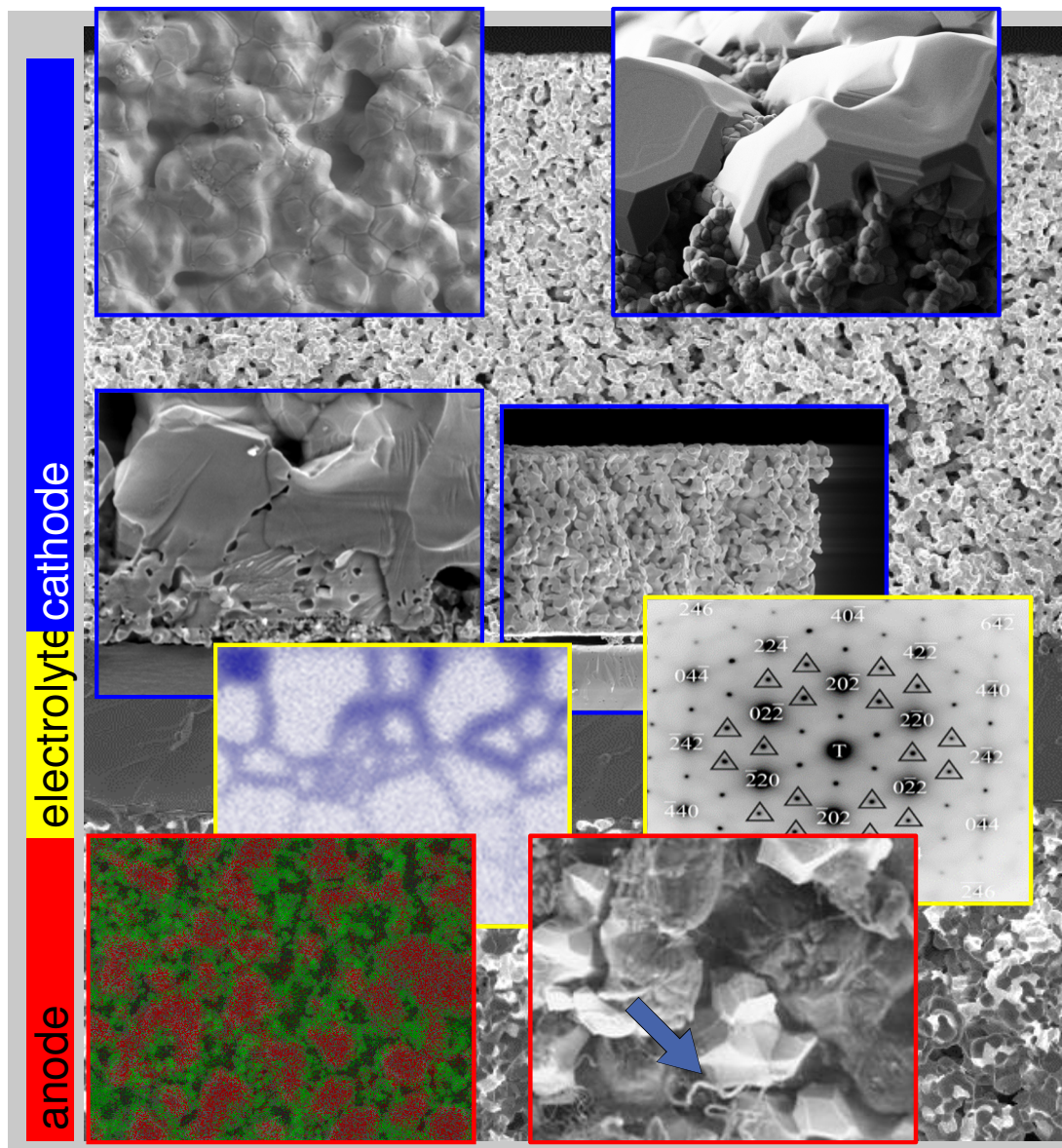


Durability Testing of Solid Oxide Cells

Research Center Jülich ASC-Stacks (2007 ff)



L. Blum et al., *ECS Trans.*, **78** (1), p. 1791 (2017)

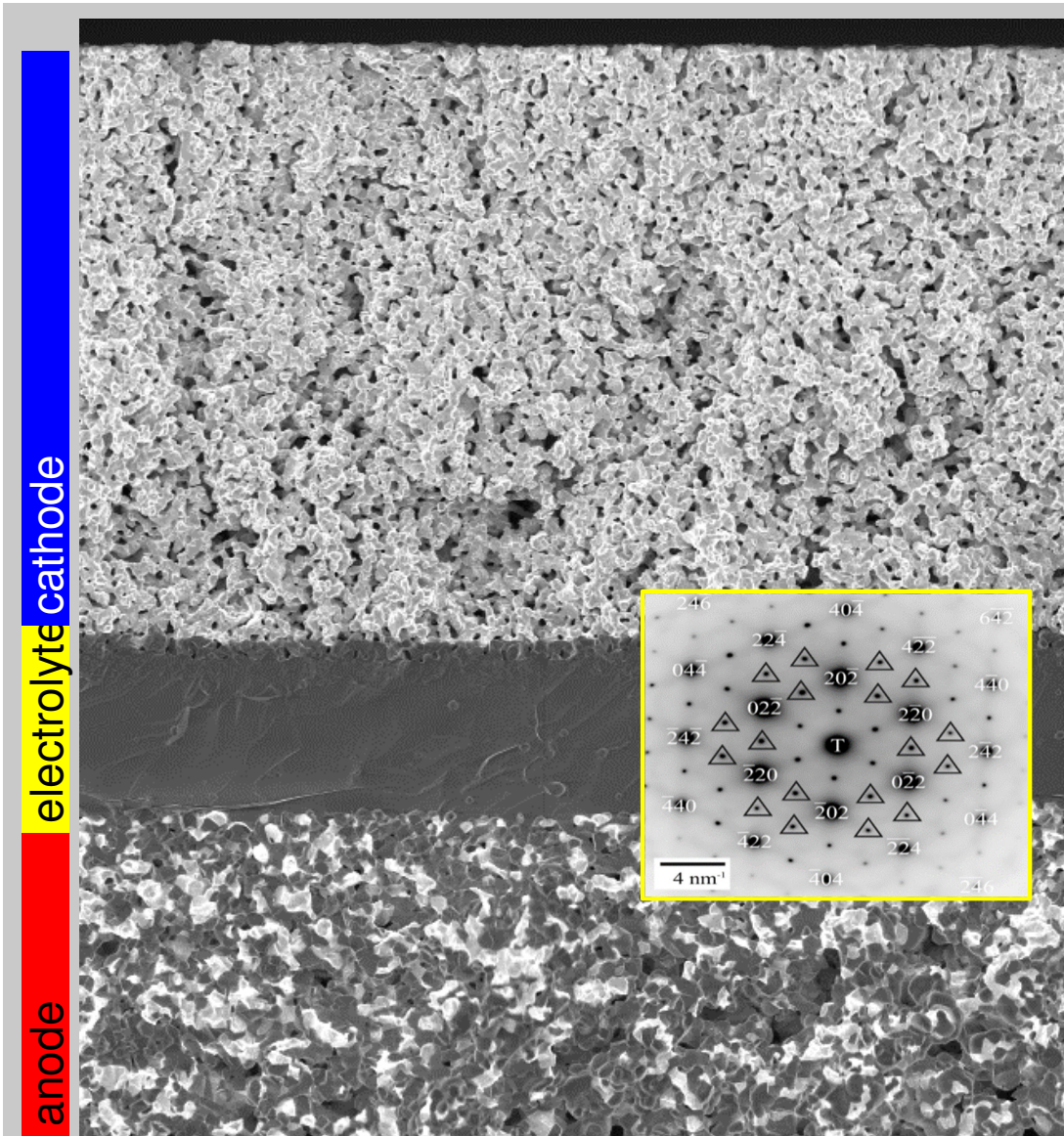


in **SOFC** many potentially competing degradation mechanisms are known:

- densification of electrodes
A. Weber et. al., *Denki Kagaku* **64**, pp. 582-589 (1996).
 - formation of micropores
 - formation of chromium compounds on the cathode
 - delamination of the cathode
M. J. Heneka et. al., *Proc. 9th Int. Symp. on SOFC*, pp. 534-543 (2005).
 - Mn-interdiffusion
A. Weber, in J. Garche (Ed.), *Encyclopedia of Electrochemical Power Sources*, Amsterdam: Elsevier, pp. 120-134 (2009).
 - intrinsic electrolyte degradation
B. Butz et. al., *Solid State Ionics* **177**, pp. 3275-3284 (2006).
 - Ni-agglomeration
A. C. Müller et. al., *Proc. 3rd European SOFC Forum*, pp. 353-362 (1998).
 - carbon deposition
E. Ivers-Tiffée et. al., *Handbook of Fuel Cells – Fundamentals, Technology and Applications*, pp. 933-956 (2009).
- ⇒ in addition, activation processes that improve the performance take place
A. Weber et. al., *Denki Kagaku* **64**, pp. 582-589 (1996).

Degradation Processes in Solid Oxide Fuel Cells

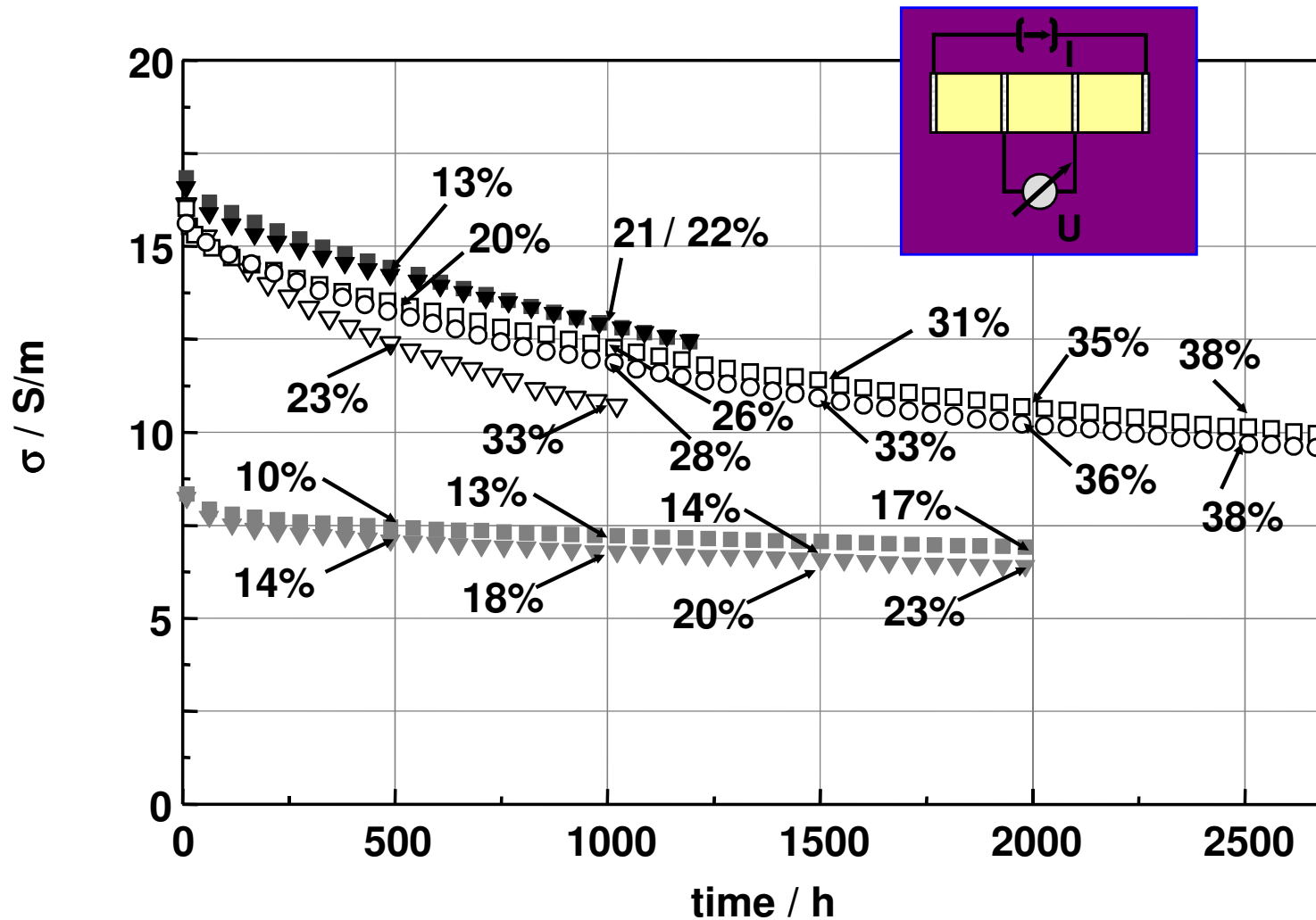
Electrolyte



- intrinsic electrolyte degradation
B. Butz et. al., *Solid State Ionics* **177**, pp. 3275-3284 (2006).

Long term stability of of ZrO₂ – Me₂O₃ Oxide Ion Conductors

FSZ: 8YSZ



$T_{op}=956^{\circ}\text{C}$, $170\text{mA}/\text{cm}^2$

○ 8YSZ, $T_{sint}=1550^{\circ}\text{C}$

□ 8YSZ, RCS @ 1500°C

▽ 8YSZ, RCS @ 1350°C

$T_{op}=956^{\circ}\text{C}$, $600\text{mA}/\text{cm}^2$

■ 8YSZ, RCS @ 1500°C

▼ 8YSZ, RCS @ 1350°C

$T_{op}=861^{\circ}\text{C}$, $120\text{mA}/\text{cm}^2$

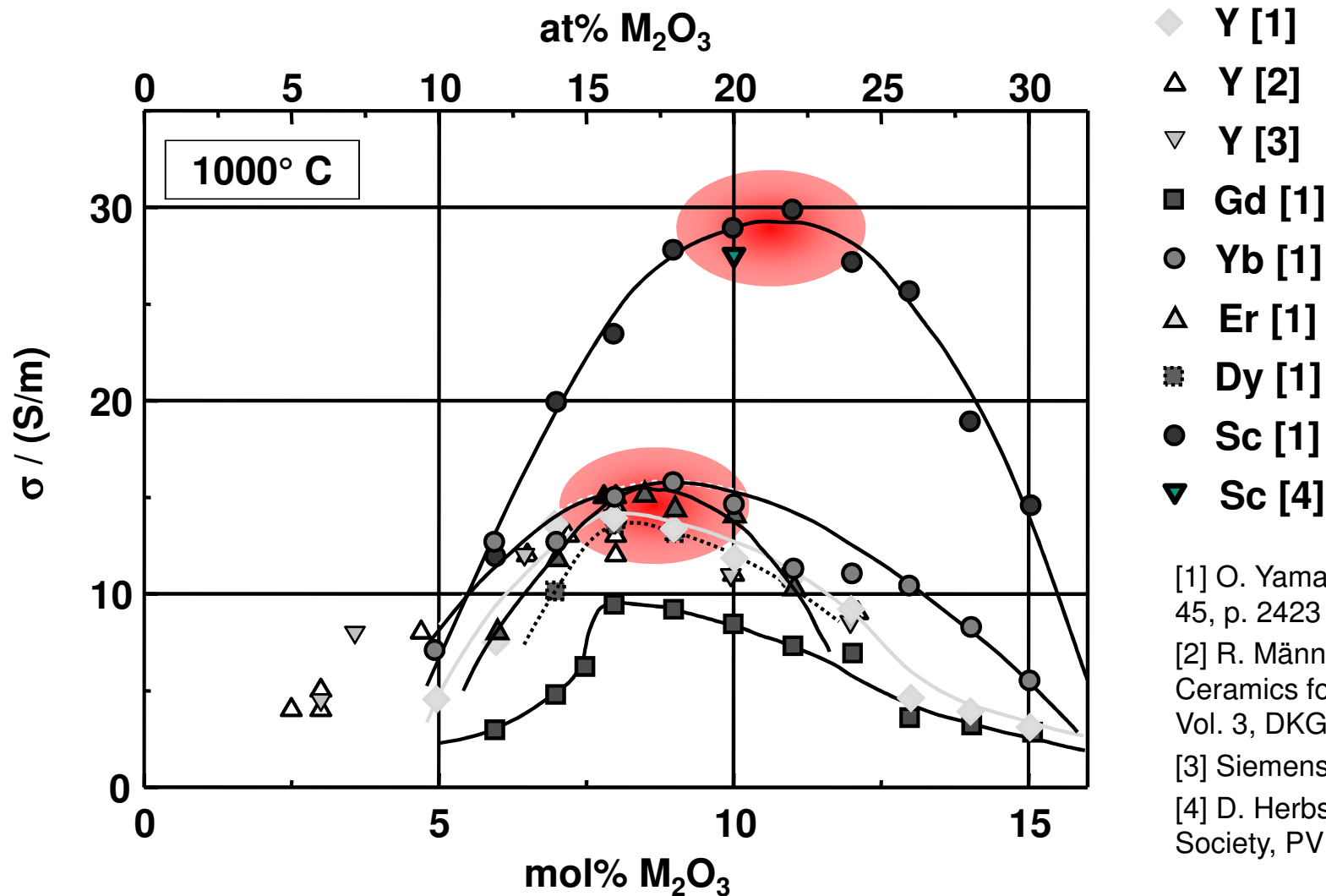
■ 8YSZ, RCS @ 1500°C

▼ 8YSZ, RCS @ 1350°C

RCS:
rate controlled sintering
constant shrinkage

Electrical Conductivity of Fluorites $\text{ZrO}_2 - \text{Me}_2\text{O}_3$

Impact of various dopants on the conductivity of ZrO_2



[1] O. Yamamoto, *Electrochimica Acta* 45, p. 2423 (2000)

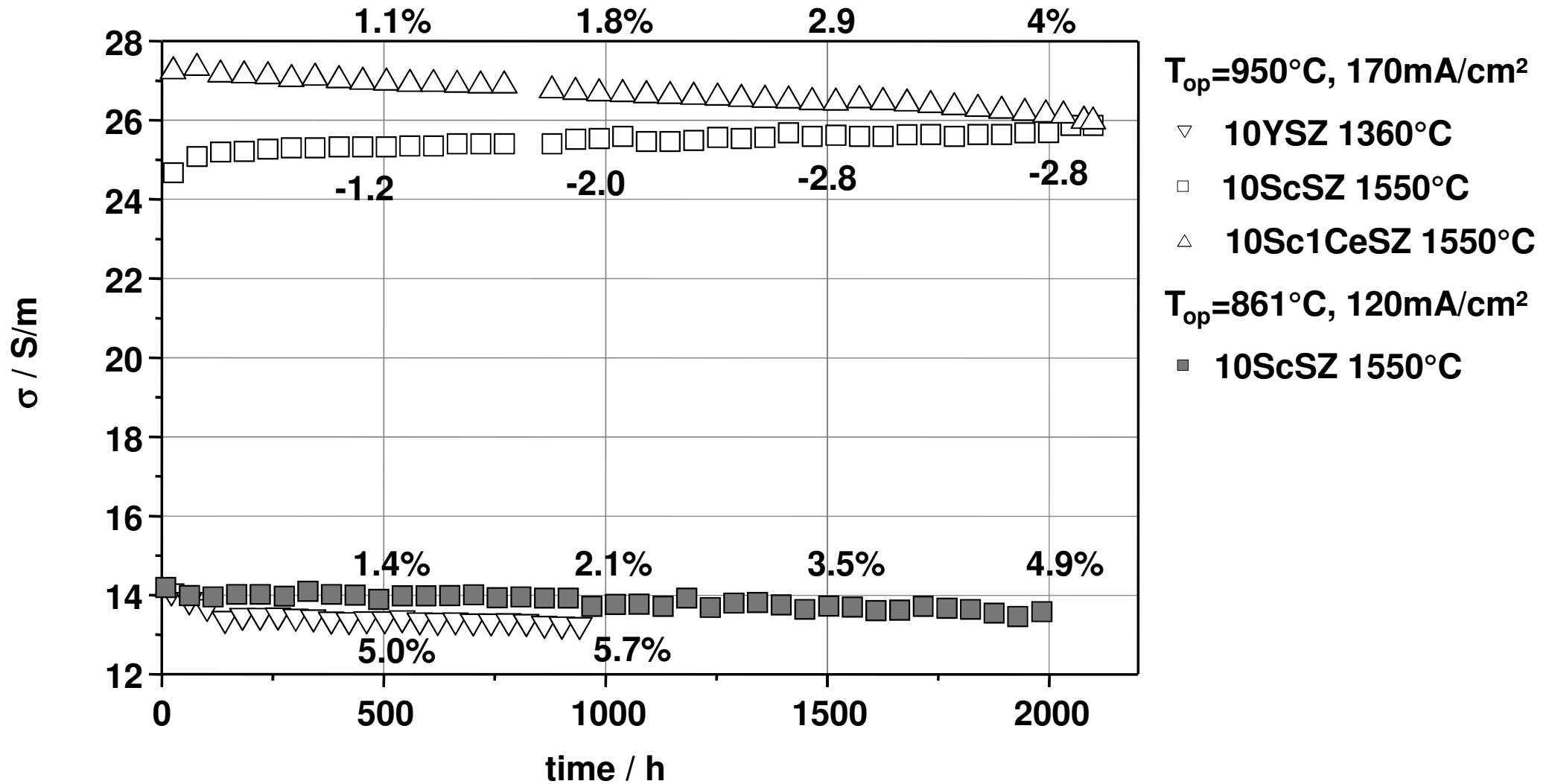
[2] R. Männer, *Electroceramics and Ceramics for Special Applications*, Vol. 3, DKG (1992)

[3] Siemens, unpublished data

[4] D. Herbstritt, *The Electrochemical Society*, PV 2001-16, p. 349, (2001)

Long term stability of of $\text{ZrO}_2 - \text{Me}_2\text{O}_3$ Oxide Ion Conductors

FSZ: 10YSZ and 10ScSZ

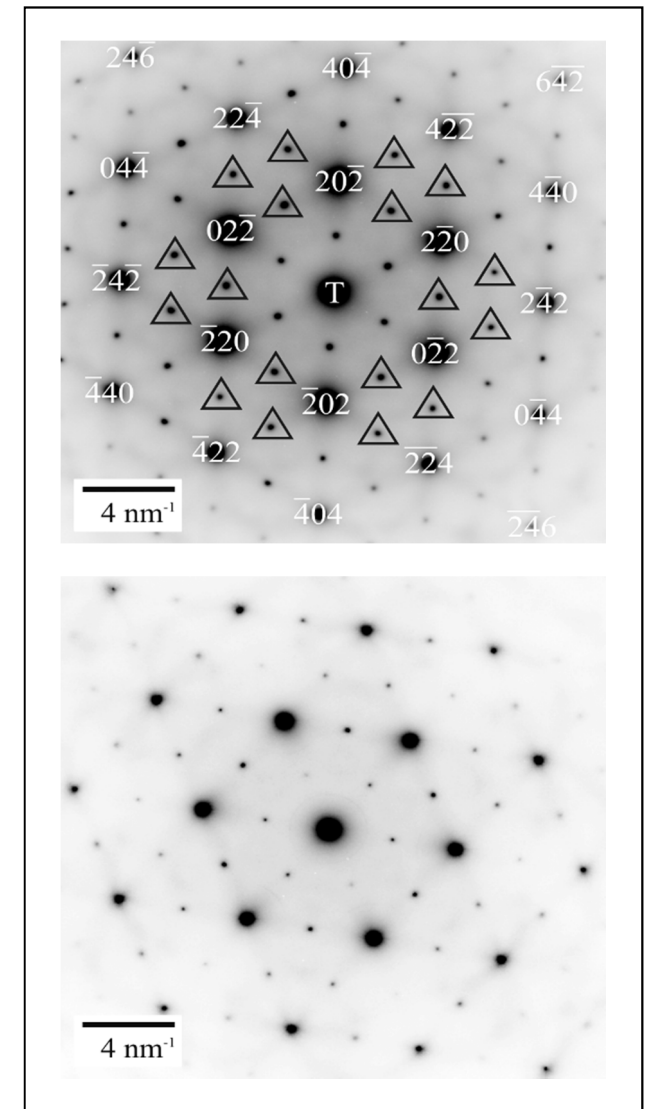


Electron diffraction: Tetragonal Phase

$[110]$, $[111]$, $[112]$, $[013]$, $[123]$

- Three variants of tetragonal phase:
c-axis along all cubic $\langle 100 \rangle$ -axes
- Double diffraction in thicker sample regions

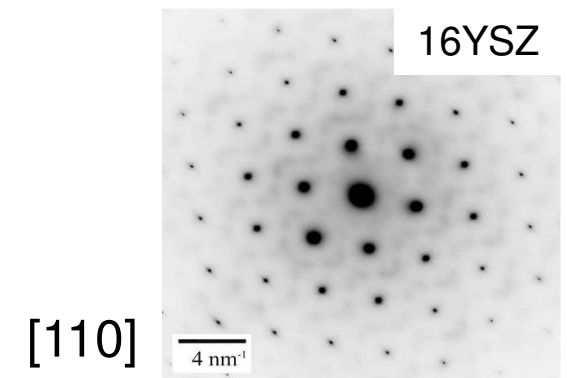
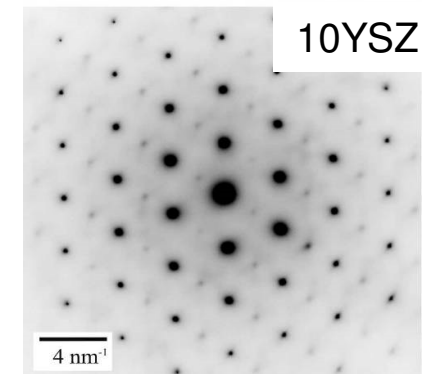
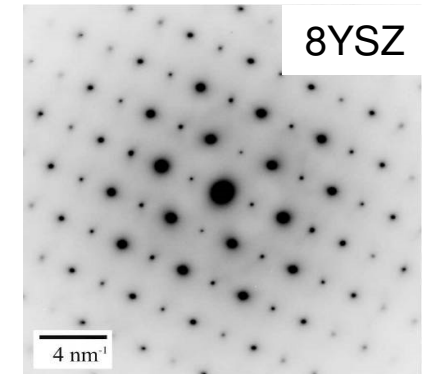
→ Clear identification of tetragonal phase
(no superstructures!)



$[111]$ 8YSZ

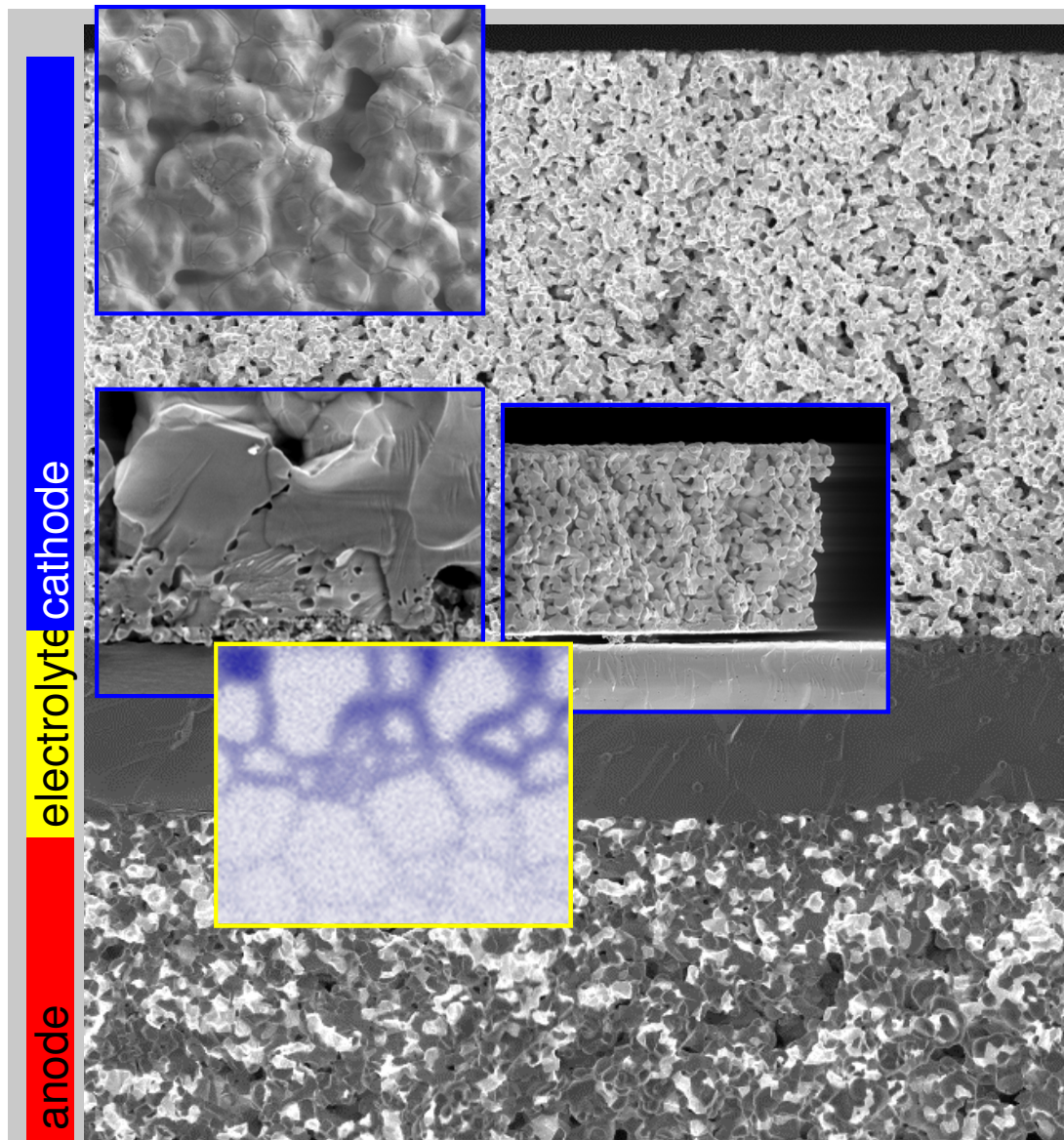
- Exists in 8YSZ and 10YSZ, not in 16YSZ
- Decreasing volume fraction with increasing doping concentration

→ Dark field images with tetragonal intensity



Degradation Processes in Solid Oxide Fuel Cells

Cathode & Cathode/Electrolyte-Interface



- densification of electrodes
- formation of micropores

A. Weber et. al., *Denki Kagaku* **64**, pp. 582-589 (1996).

- delamination of the cathode

M. J. Heneka et. al., Proc. 9th Int. Symp. on SOFC, pp. 534-543 (2005).

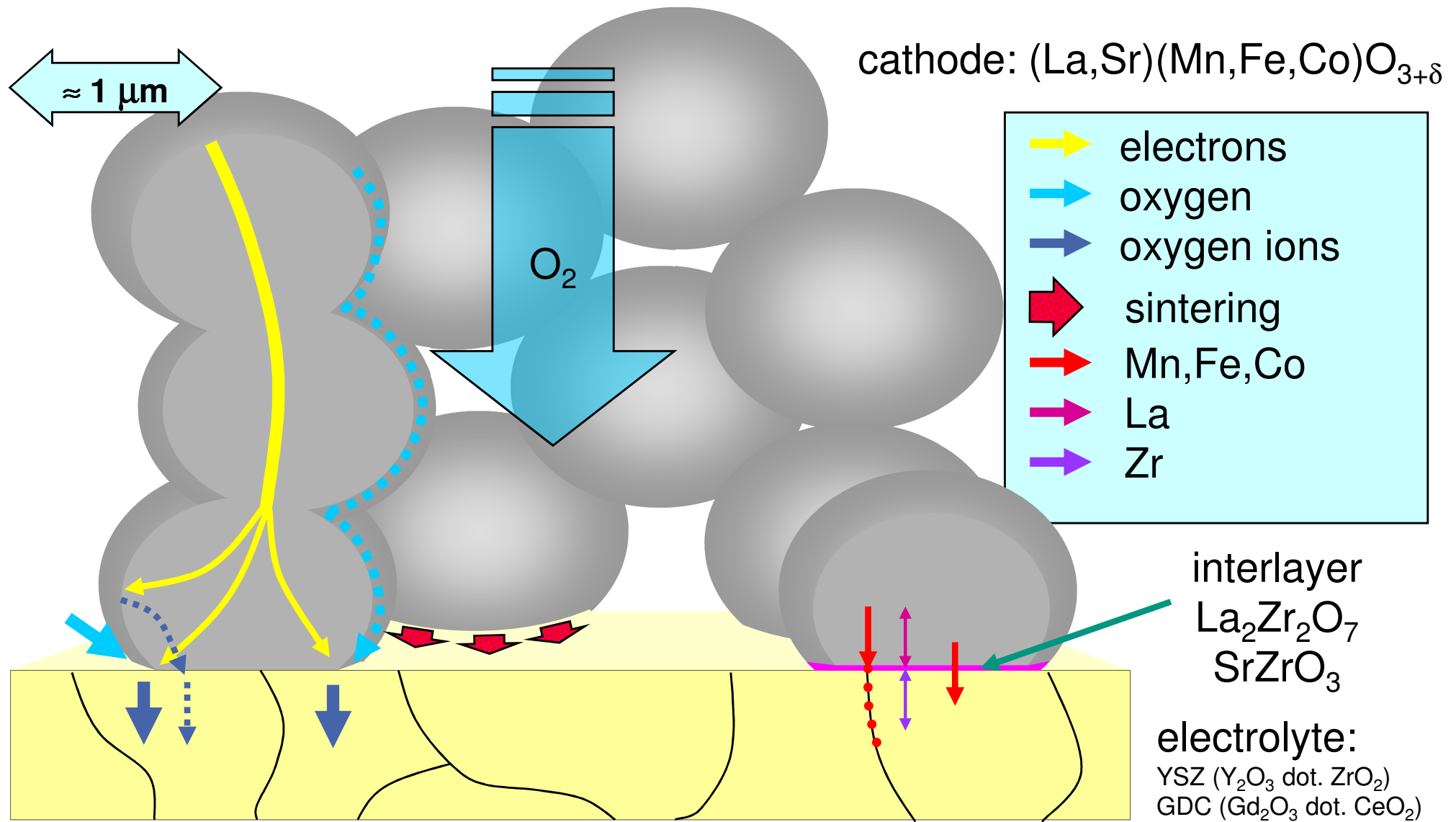
- Mn-interdiffusion

A. Weber, in J. Garche (Ed.), Encyclopedia of Electrochemical Power Sources, Amsterdam: Elsevier, pp. 120-134 (2009).

⇒ in addition, activation processes that improve the performance take place

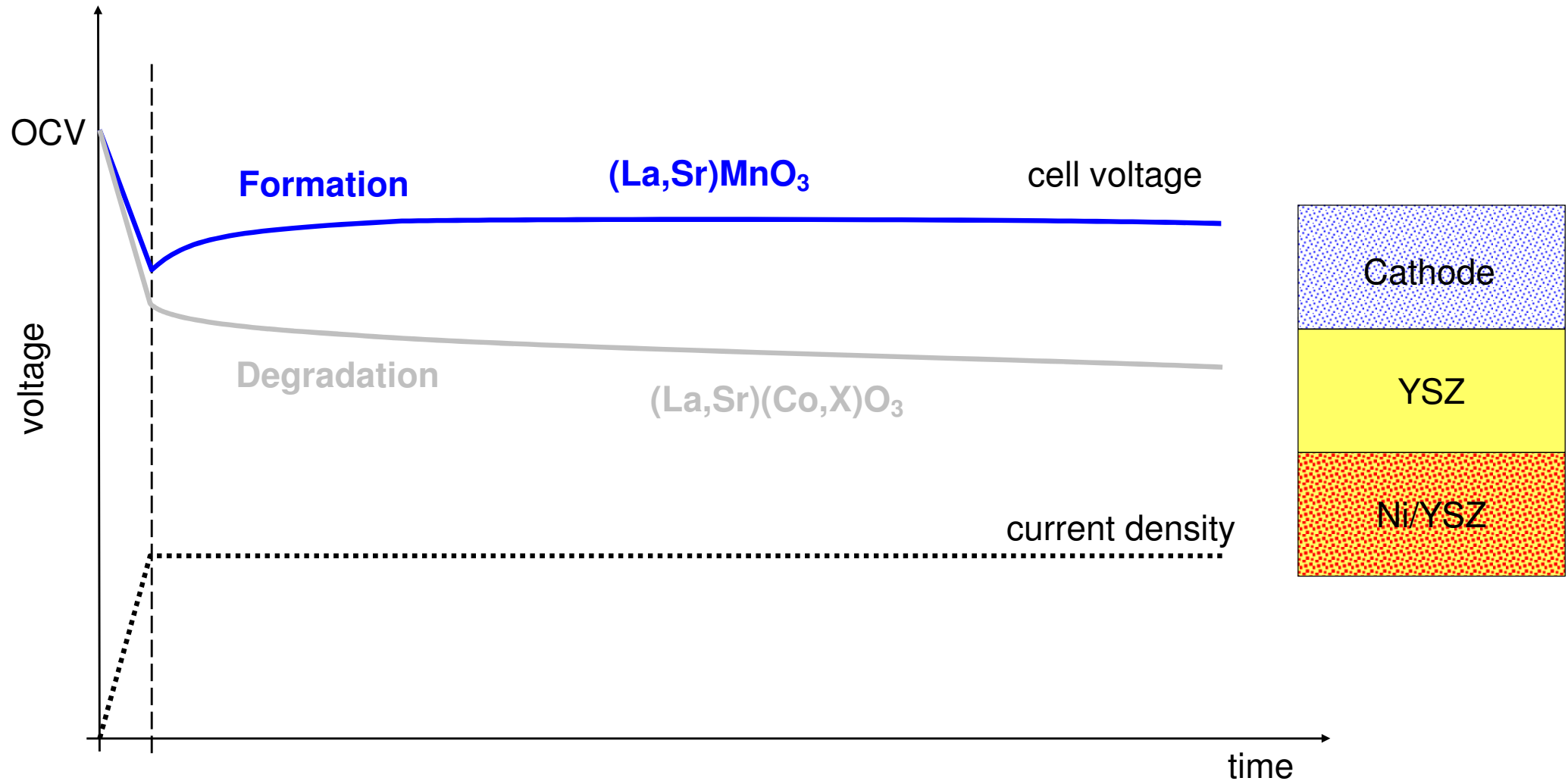
A. Weber et. al., *Denki Kagaku* **64**, pp. 582-589 (1996).

Stability of Interfaces



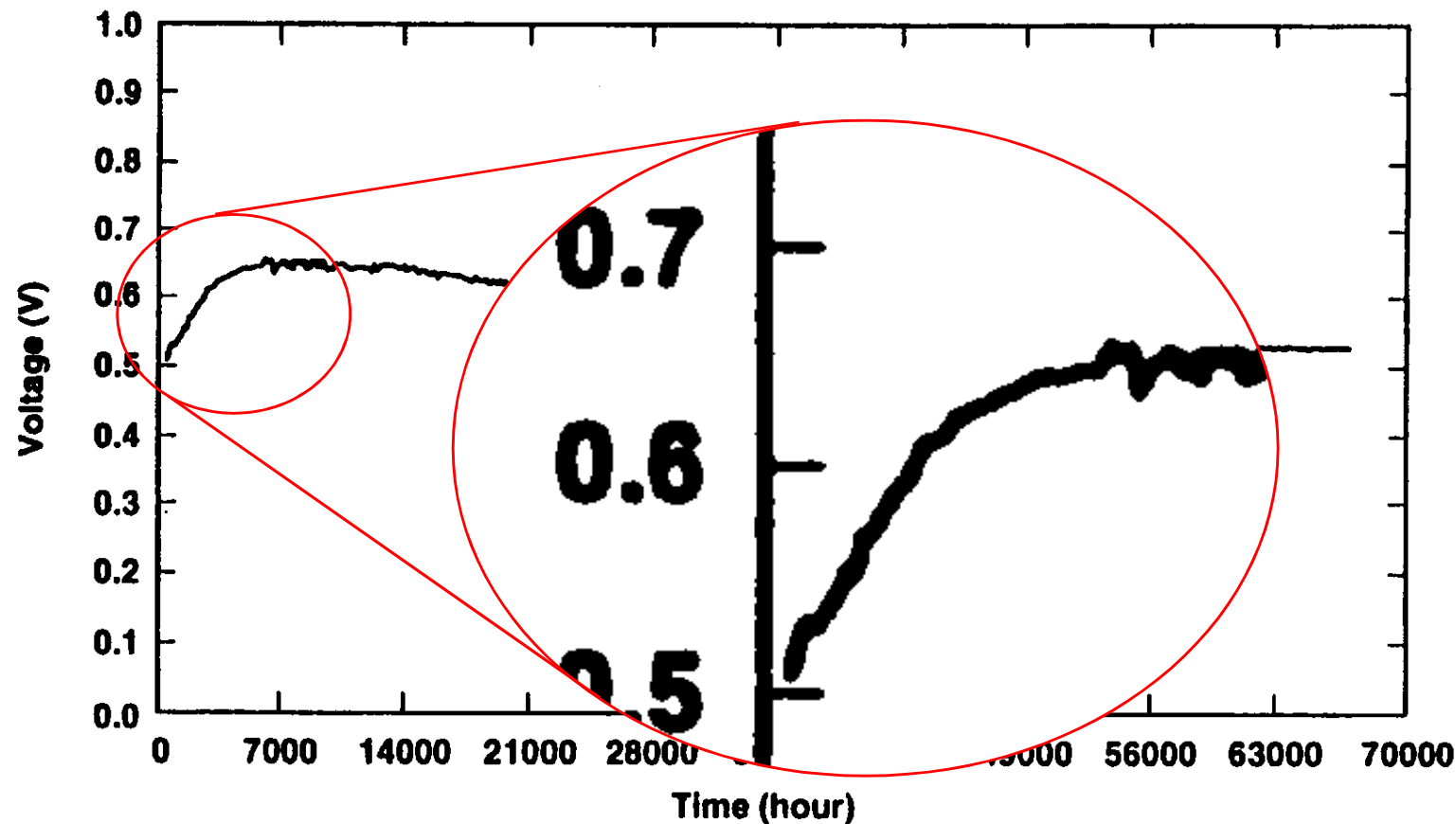
Startup Behavior of SOFC Single Cells and Stacks

Formation and Degradation



SOFC: Formation and Long Term Test of a tubular Cell

Siemens-Westinghouse SWPC (1997)



$V_{\text{start}} : 0.50 \text{ V}$

$V_{\text{max}} : 0.65 \text{ V}$

► V_{max} : Point of max. performance

► time to V_{max} :
 $\approx 5.000 \text{ hours}$

Fig. 1. Long term test of an early-technology PST cell.

S. C. Singhal, Recent Progress in Tubular Solid Oxide Fuel Cell Technology, Proc. 5th Int. Symposium on SOFC, Ed. U. Stimming, S. C. Singhal, H. Tagawa, W. Lehnert, The Electrochemical Society, PV 97-40, 37-50, (1997)

SOFC: Formation and Long Term Test of a 5-cell Stack

Sulzer Hexis (1999)

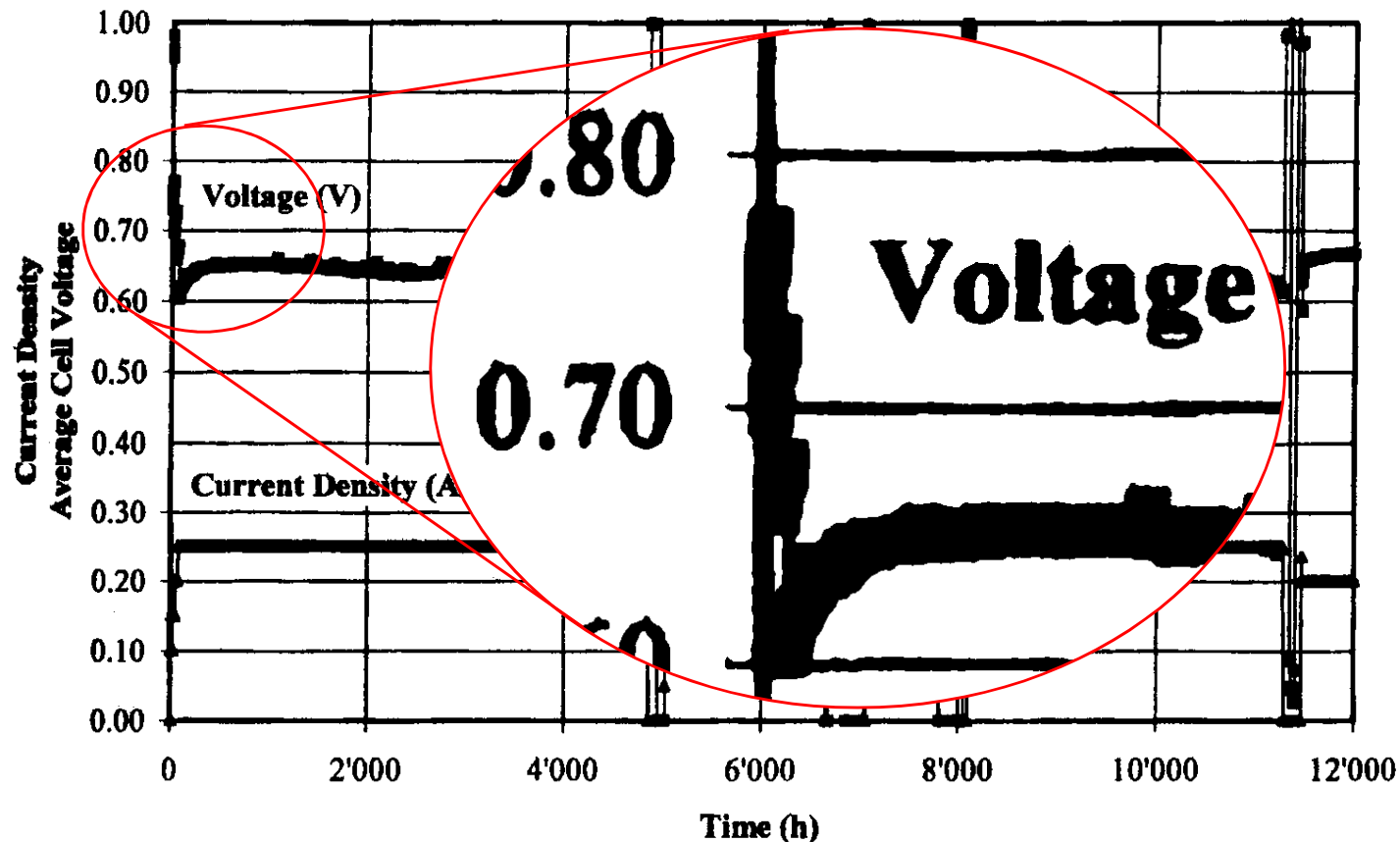


Figure 2: Negligible degradation of a five cell stack

$V_{\text{start}} : 0.60 \text{ V}$

$V_{\text{max}} : 0.65 \text{ V}$

► V_{max} : Point of max. performance

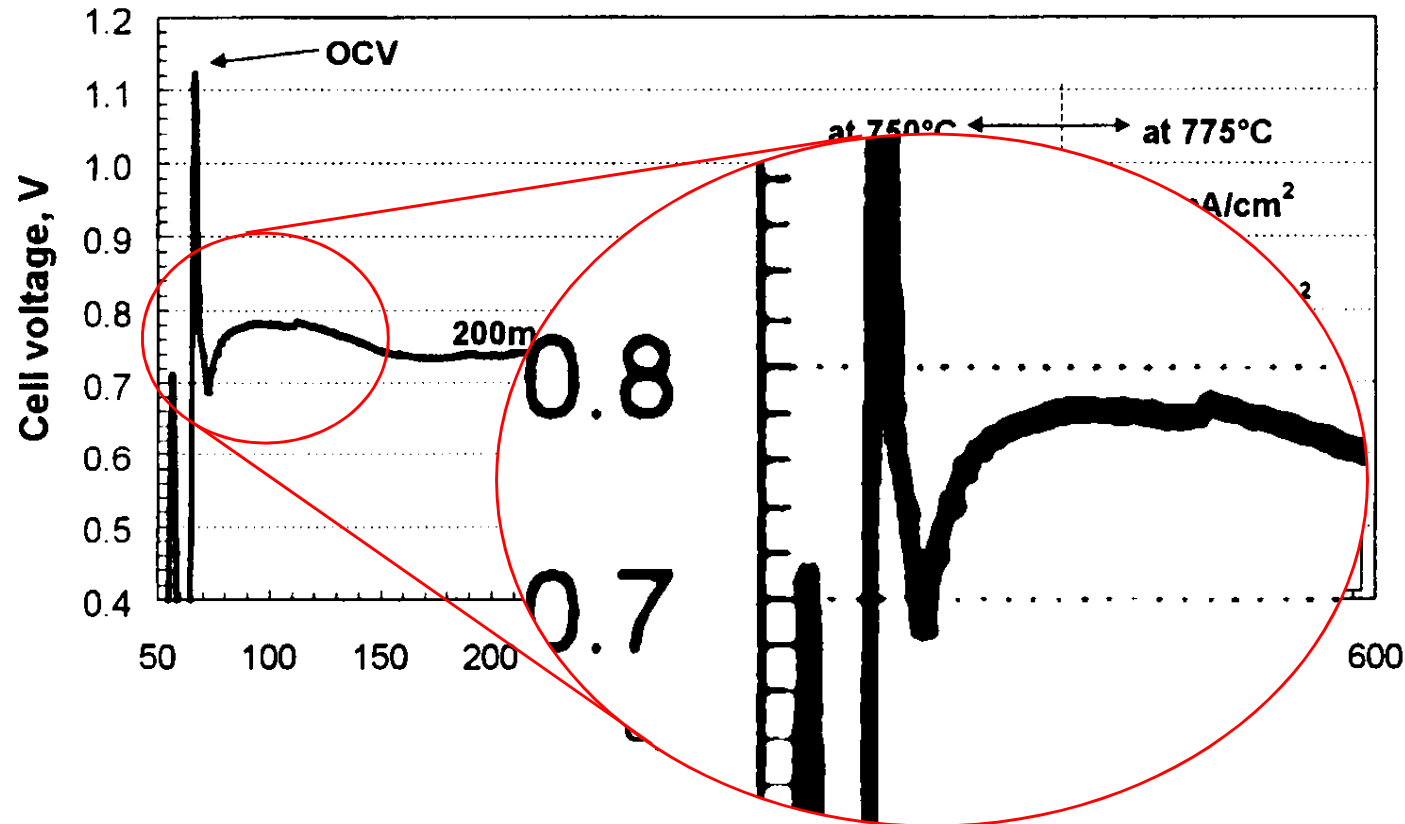
► time to V_{max} :

$\approx 200 \text{ hours}$

R. Diethelm, M. Schmidt, Status of the Sulzer Hexis Product Development, Proc. 6th Int. Symp. on SOFC, Ed. S. Singhal und M. Dokiya, The Electrochemical Society, PV 99-19, 60-67, (1999)

SOFC: Formation and Long Term Test of a planar Cell

Ceramic Fuel Cells Ltd. CFCL (1999)



$V_{\text{start}} : 0.68 \text{ V}$

$V_{\text{max}} : 0.78 \text{ V}$

► V_{max} : Point of
max. performance

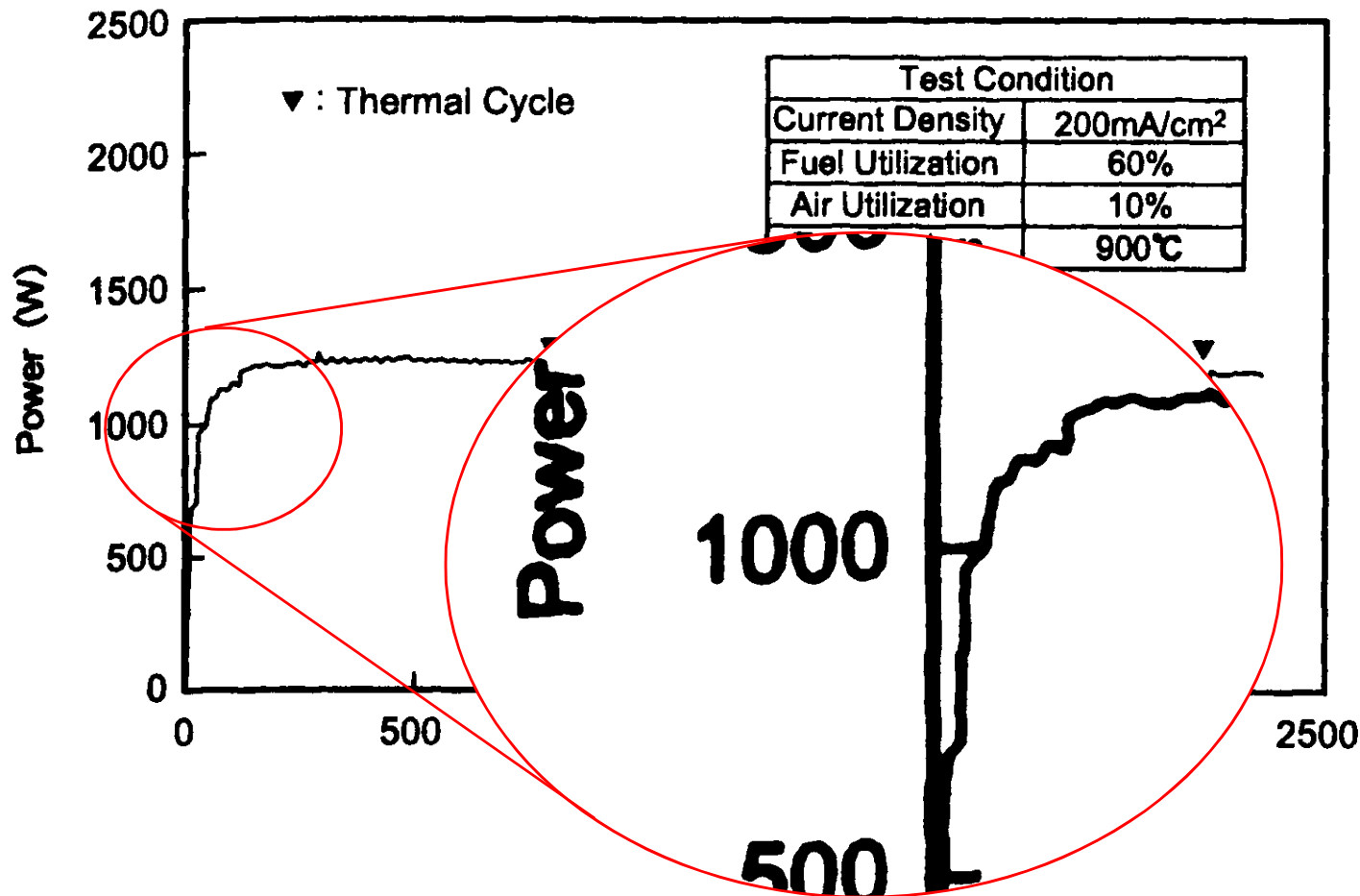
► time to V_{max} :
 $\approx 50 \text{ hours}$

Figure 2. Cell performance at 750 and 775°C tested in alumina assembly

K. Föger et al., Demonstration of Anode Supported Cell Technology in kW Class Stack, Proc. 6th Int. Symp. on SOFC, Ed. S. Singhal und M. Dokiya, The Electrochemical Society, 95-100, PV 99-19, (1999)

SOFC: Formation and Long Term Test of a 1 kW Stack

Mitsubishi Heavy Industries MHI (1999)



P_{start} : 700 W

P_{max} : 1250 W

► P_{max} : Point of max. performance

► time to P_{max} :
 $\approx$ 300 hours

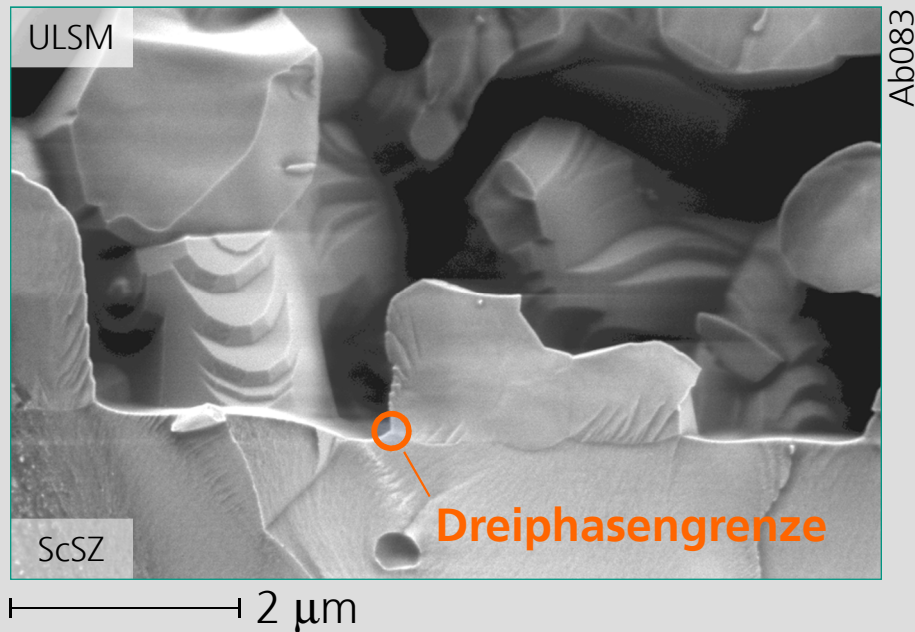
Fig. 12 Endurance Test of 1kW Module with Co-Sintered Cell Stack

H. Mori et al., Pressurized 10 kW Class Module of SOFC, Proc. 6th Int. Symp. on SOFC, Ed. S. Singhal und M. Dokiya, - The Electrochemical Society, PV 99-19, 52-59, (1999)

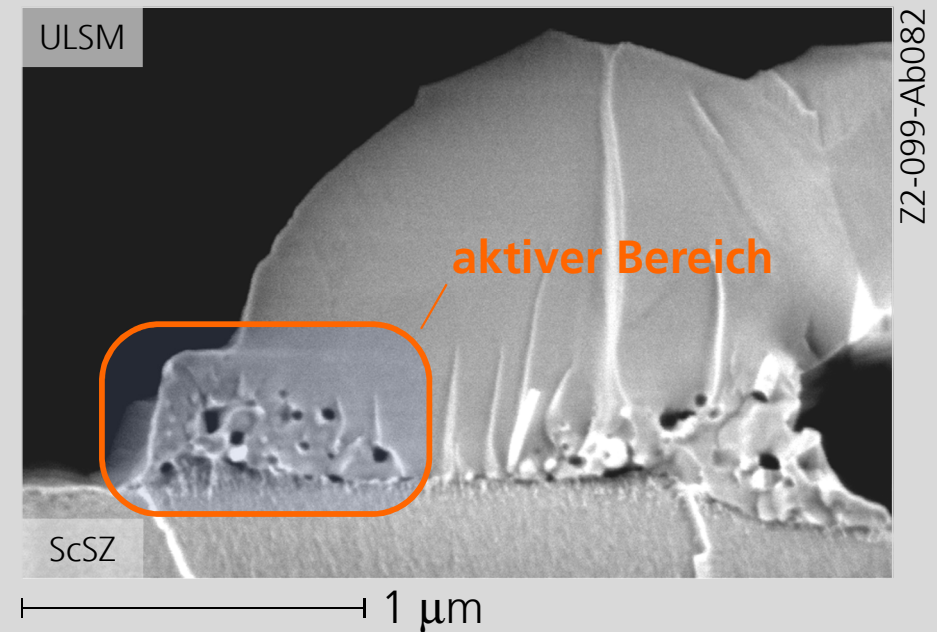
Grenzfläche Kathode-Elektrolyt vor und nach Aktivierung

Mikrostruktur

unbelastete MEA



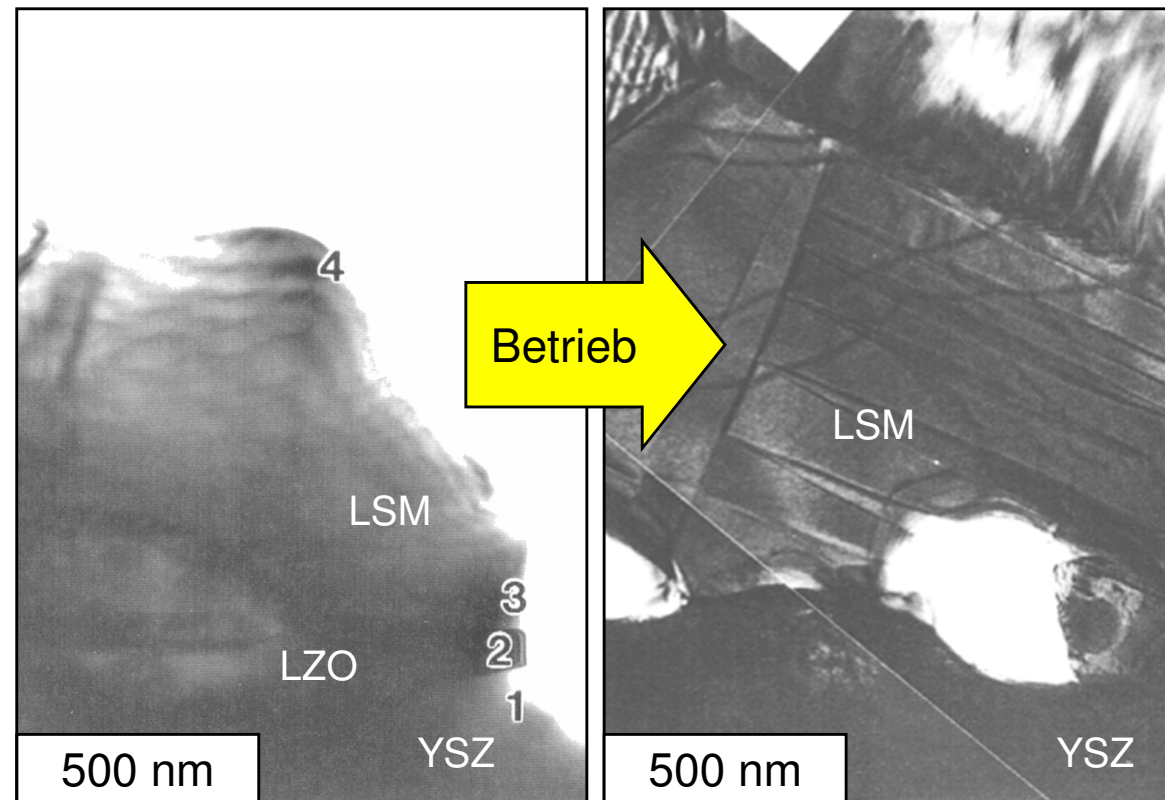
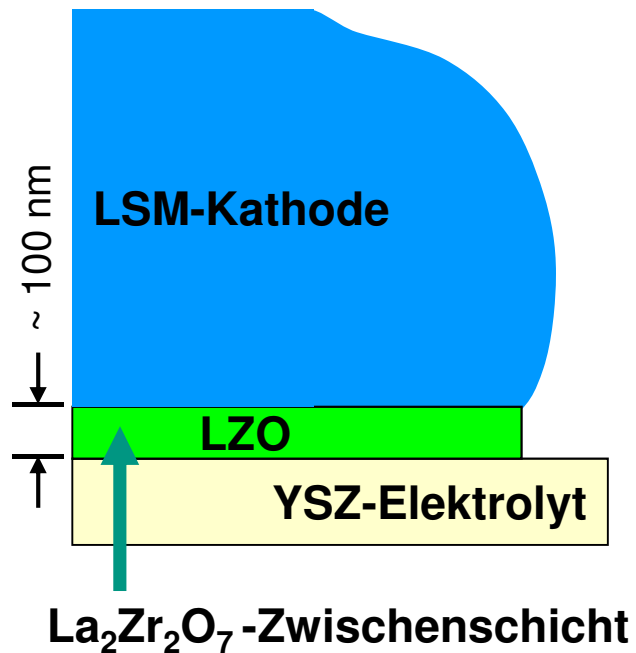
nach Aktivierung



- Bildung eines porösen Bereichs im ULSM-Korn nahe der Grenzfläche unter Belastung
- Reaktionsraum vergrößert $\Rightarrow$ höhere elektrochemische Leistungsfähigkeit der Kathode

Grenzfläche Kathode-Elektrolyt vor und nach Aktivierung

Chemische Zusammensetzung

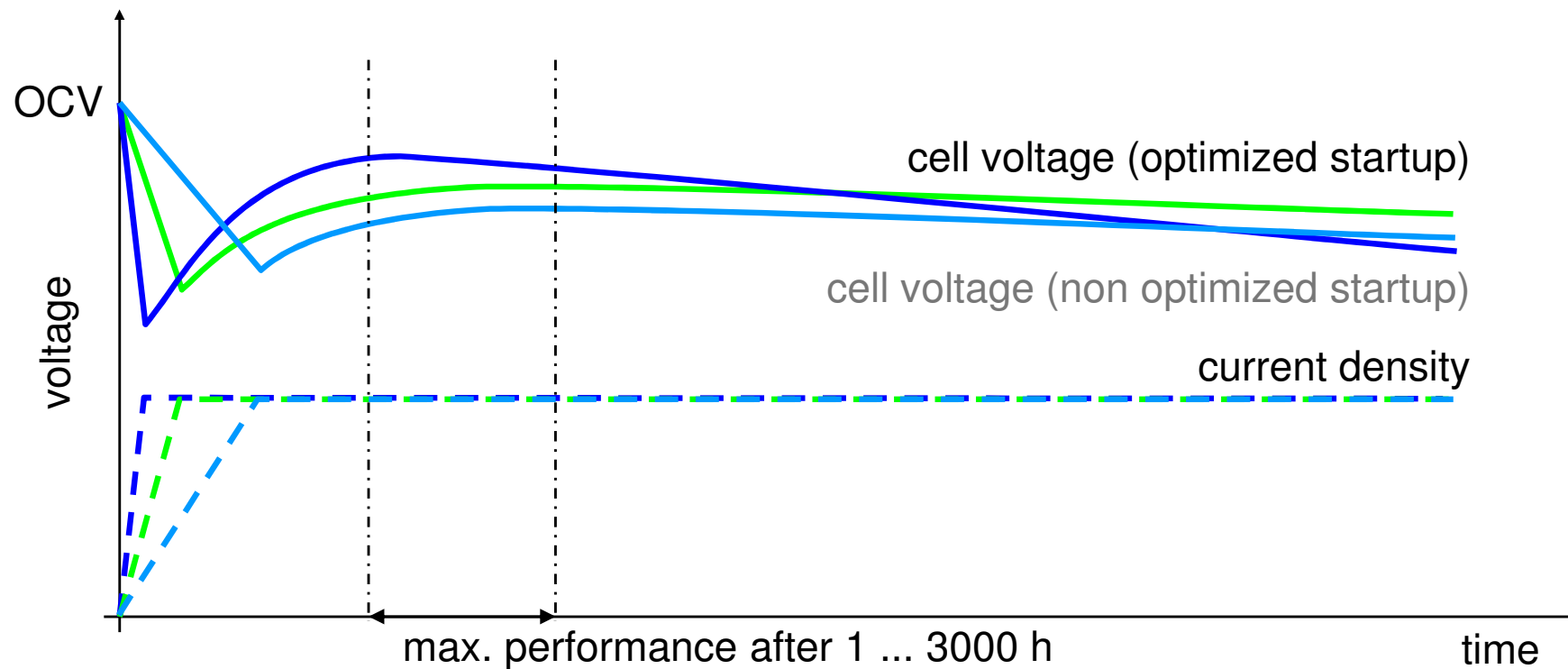


• Abbau der La₂Zr₂O₇-Zwischenschicht

Startup Behavior of SOFC Single Cells and Stacks

Formation and Degradation

	max. performance	degradation
— (dark blue)	++	-
— (green)	+	+
— (light blue)	-	+



Modeling of Degradation Phenomena

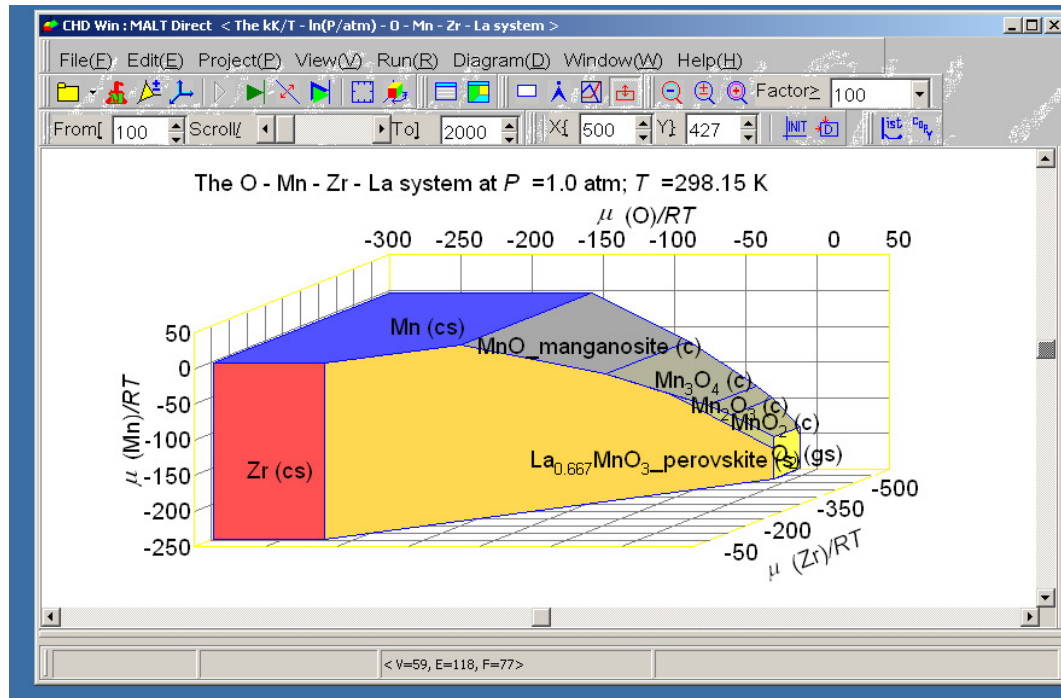
Chemical Potential Diagrams and Thermodynamic Equilibrium Calculations

MALT (MAterials oriented Little Thermodynamic database*)

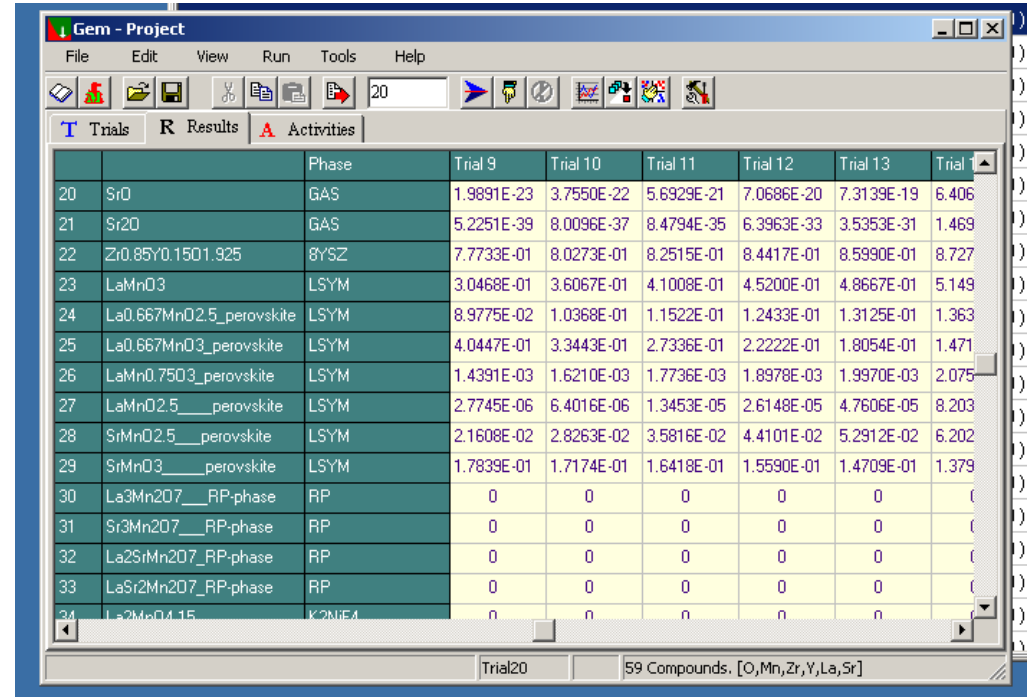
$$\Delta_f G^\circ, \Delta_f H^\circ, S^\circ, C_p^\circ \text{ at } 298.15 \text{ K}$$

temperature coefficients of heat capacities, transition temperatures, transition enthalpies

Calculation of Chemical Potential Diagrams (CHD)



Thermodynamic Equilibrium Calculations (GEM: Gibbs Energy Minimizer)

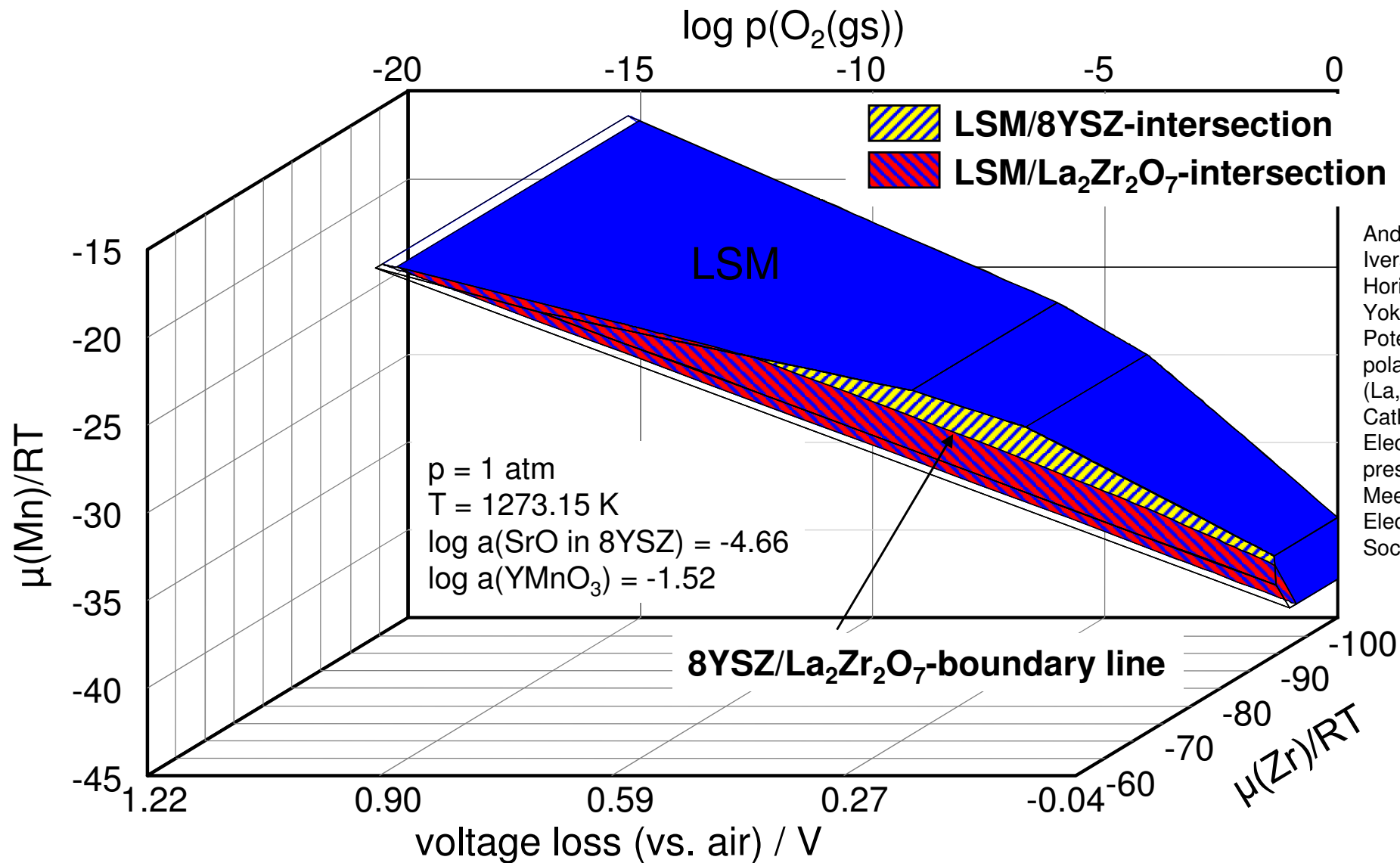


	Phase	Trial 9	Trial 10	Trial 11	Trial 12	Trial 13	Trial 14
20	SrO	GAS	1.9891E-23	3.7550E-22	5.6929E-21	7.0686E-20	7.3139E-19
21	Sr2O	GAS	5.2251E-39	8.0096E-37	8.4794E-35	6.3963E-33	3.5353E-31
22	Zr0.85Y0.15O1.925	8YSZ	7.7733E-01	8.0273E-01	8.2515E-01	8.4417E-01	8.5990E-01
23	LaMnO3	LSYM	3.0468E-01	3.6067E-01	4.1008E-01	4.5200E-01	4.8667E-01
24	La0.667MnO2.5_perovskite	LSYM	8.9775E-02	1.0368E-01	1.1522E-01	1.2433E-01	1.3125E-01
25	La0.667MnO3_perovskite	LSYM	4.0447E-01	3.3443E-01	2.7336E-01	2.2222E-01	1.8054E-01
26	LaMn0.75O3_perovskite	LSYM	1.4391E-03	1.6210E-03	1.7736E-03	1.8978E-03	1.9970E-03
27	LaMnO2.5_perovskite	LSYM	2.7745E-06	6.4016E-06	1.3453E-05	2.6148E-05	4.7606E-05
28	SrMnO2.5_perovskite	LSYM	2.1608E-02	2.8263E-02	3.5816E-02	4.4101E-02	5.2912E-02
29	SrMnO3_perovskite	LSYM	1.7839E-01	1.7174E-01	1.6418E-01	1.5590E-01	1.4709E-01
30	La3Mn2O7_RP-phase	RP	0	0	0	0	0
31	Sr3Mn2O7_RP-phase	RP	0	0	0	0	0
32	La2SrMn2O7_RP-phase	RP	0	0	0	0	0
33	LaSr2Mn2O7_RP-phase	RP	0	0	0	0	0
34	La2MnO4.15	K2NIE4	0	0	0	0	0

* H. Yokokawa et al., Thermochimica Acta 245, 45-55 (1994)
MALT for Windows, see <http://www.kagaku.com/malt/index.html>

Modeling of Degradation Phenomena

Chemical Potential Diagram for the polarized LSM / 8YSZ - Interface

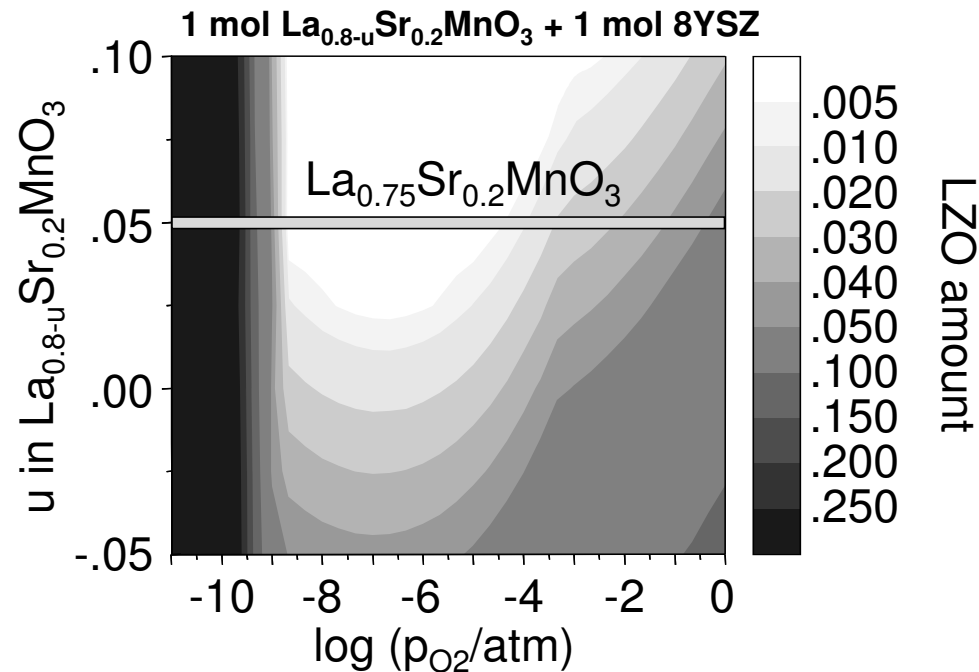


André Weber, Ellen Ivers-Tiffée, Teruhisa Horita, Harumi Yokokawa, Chemical Potential Diagrams for polarized (La,Sr)MnO_{3+d}-Cathode/8YSZ-Electrolyte-Interfaces", presented at the 206th Meeting of The Electrochemical Society, 2004

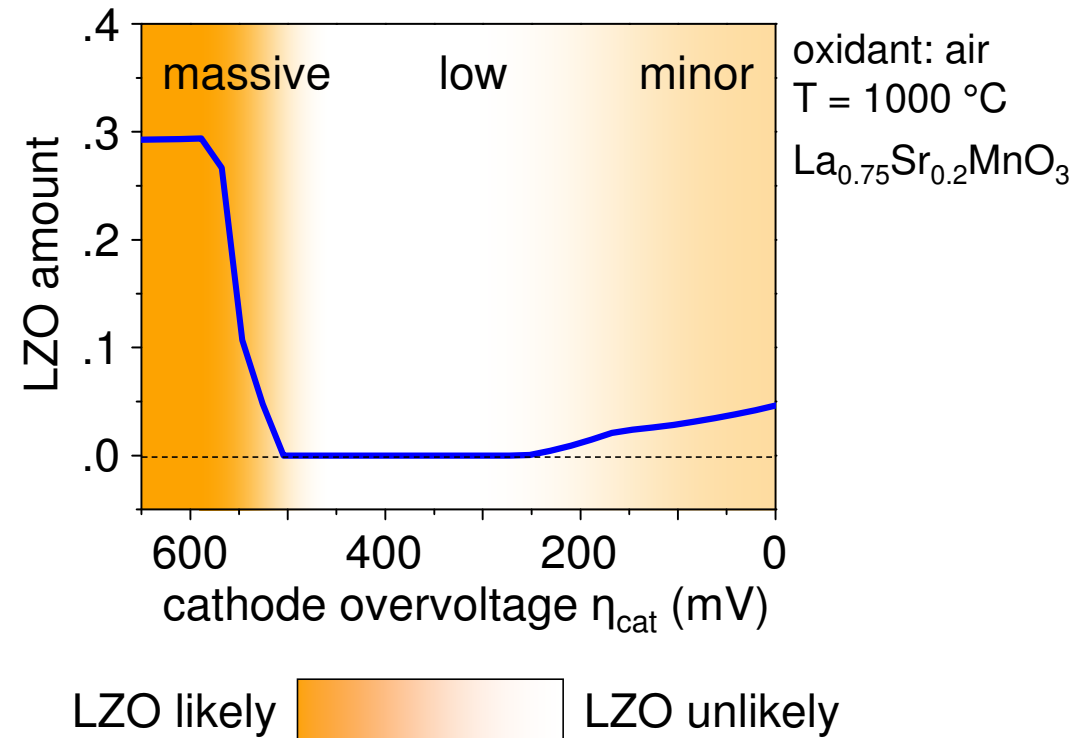
Modeling of Degradation Phenomena

Formation of insulating LZO-layers at the LSM/8YSZ Interface

calculated amount of LZO



impact of cathode overvoltage η_{cat}

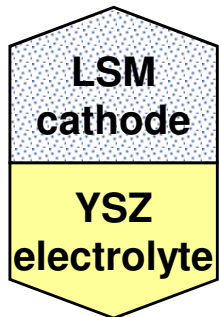
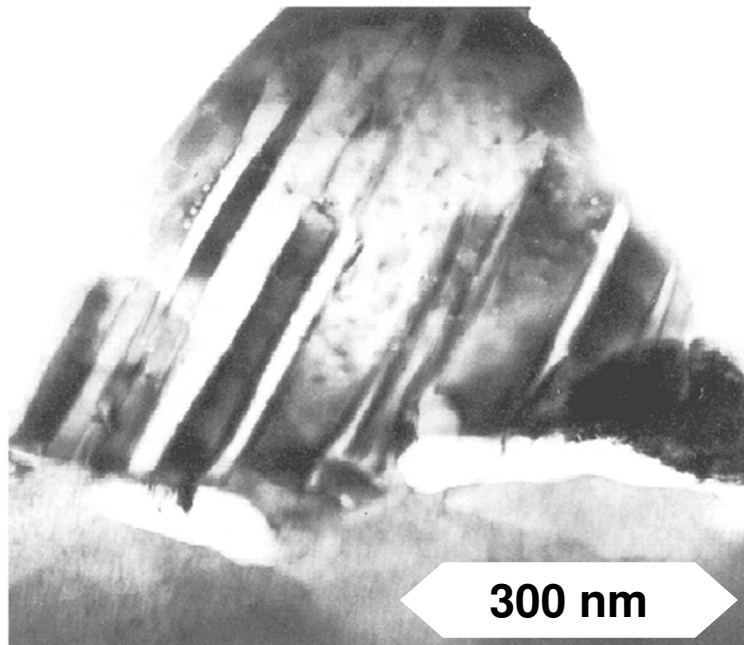


M. J. Heneka, E. Ivers-Tiffée: Degradation of SOFC Single Cells Under Severe Current Cycles. In: S. C. Singhal, J. Mizusaki (Hrsg.), Proc. 9th Int. Symp. on SOFC, PV 2005-07, The Electrochemical Society, 534-543 (2005)

Cathode Degradation

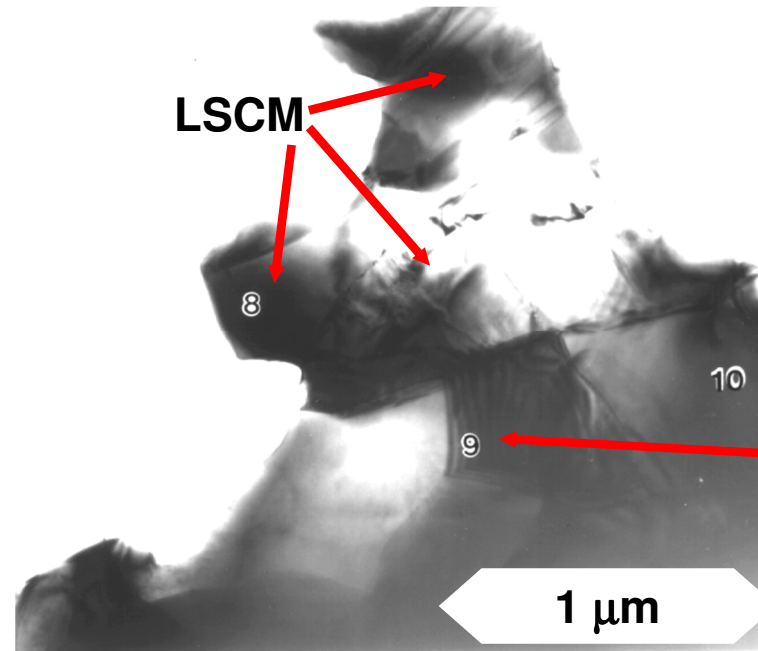
Growth of Secondary Phases at the Cathode/Electrolyte-Interface

Interface LSM/YSZ
(LSM: $\text{La}_{0.8}\text{Sr}_{0.2}\text{MnO}_{3+\delta}$)



Low Cathode Resistance
after Formation

Interface LSCM/YSZ
(LSCM: $\text{La}_{0.8}\text{Sr}_{0.2}\text{Co}_{0.5}\text{Mn}_{0.5}\text{O}_{3+\delta}$)

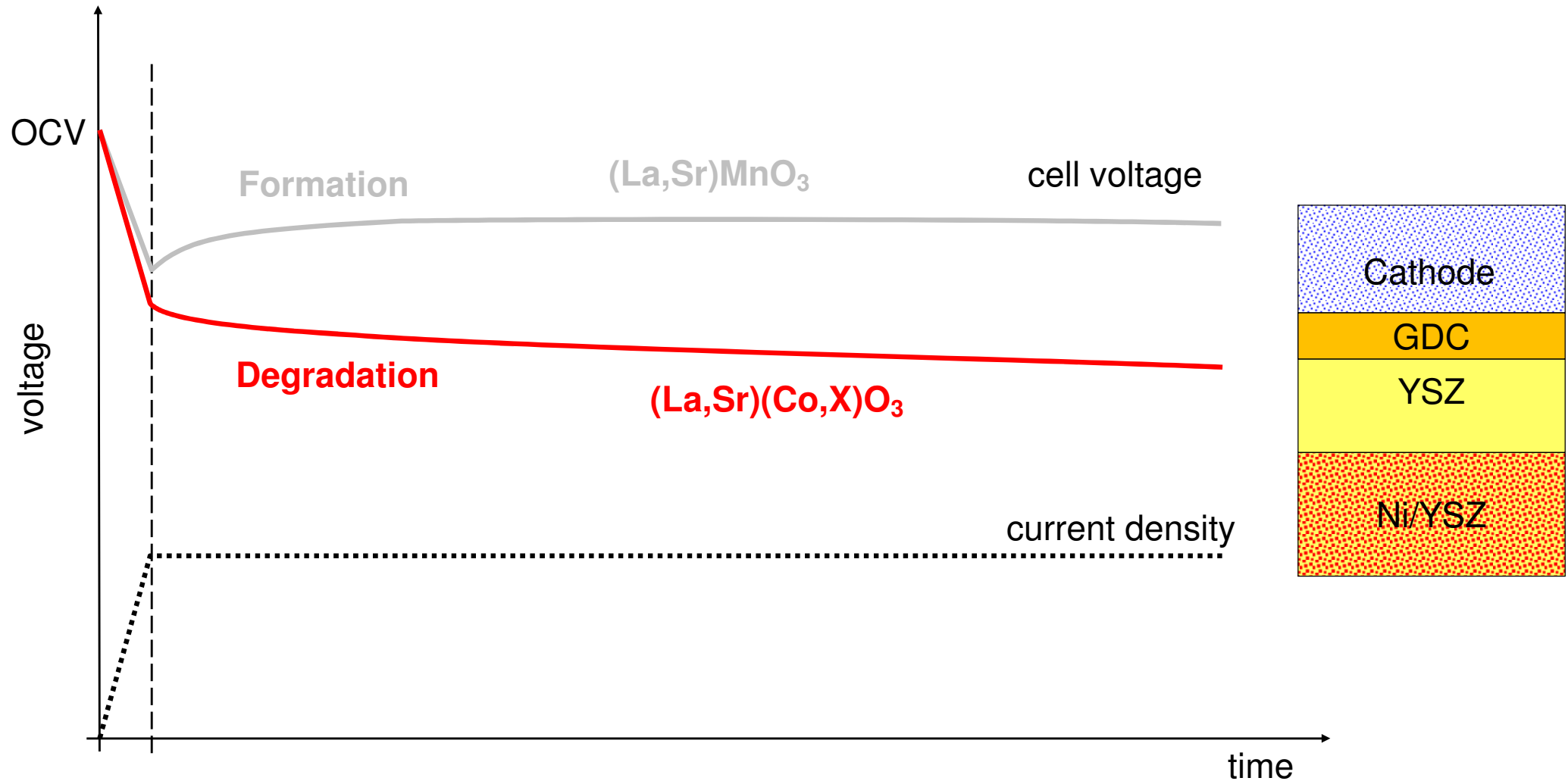


High Cathode Resistance
Growth of Secondary Phases

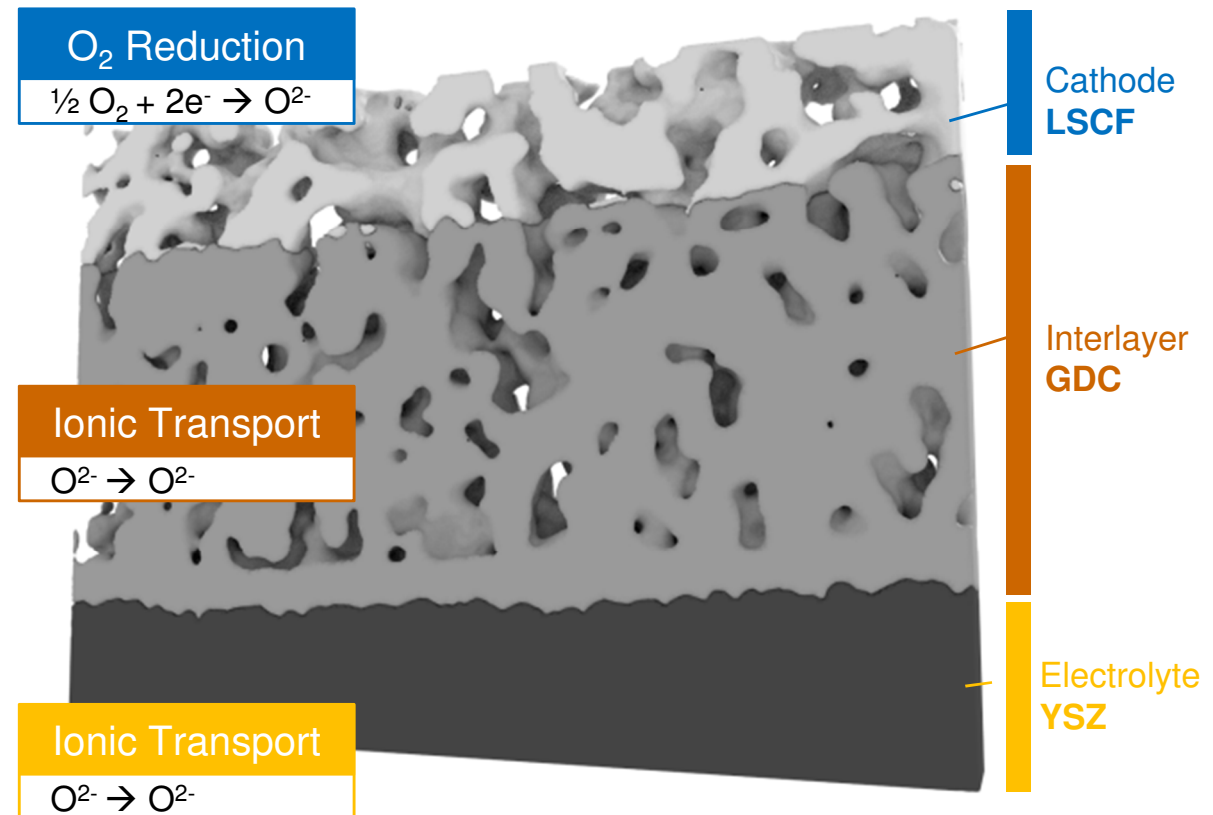
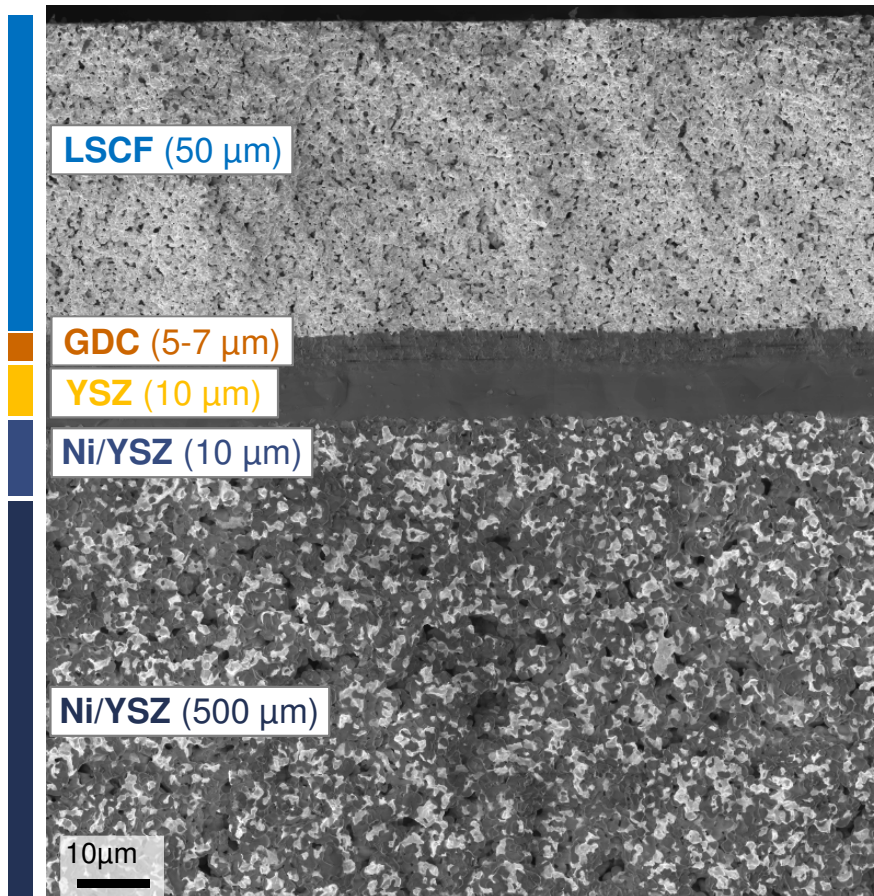


Startup Behavior of SOFC Single Cells and Stacks

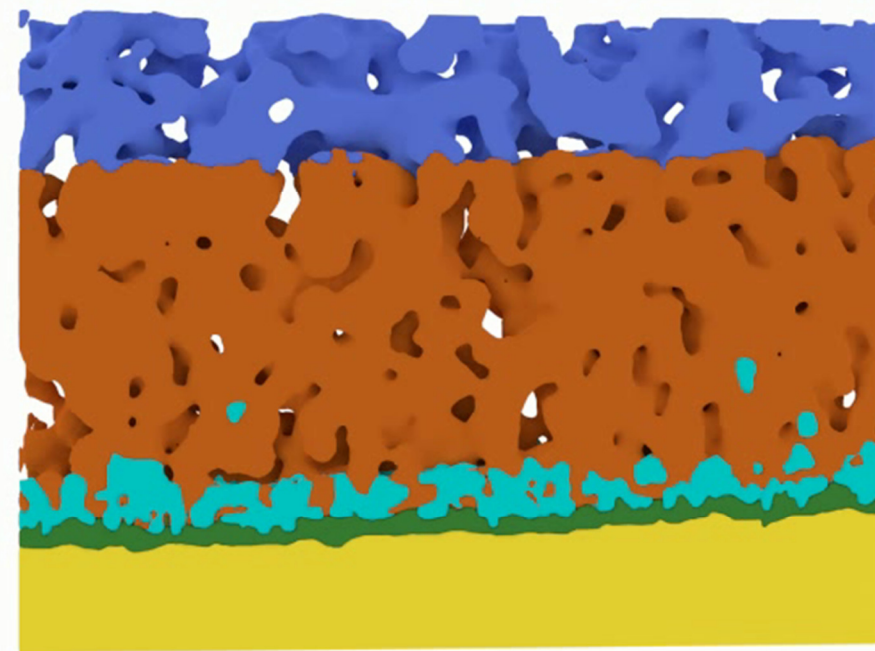
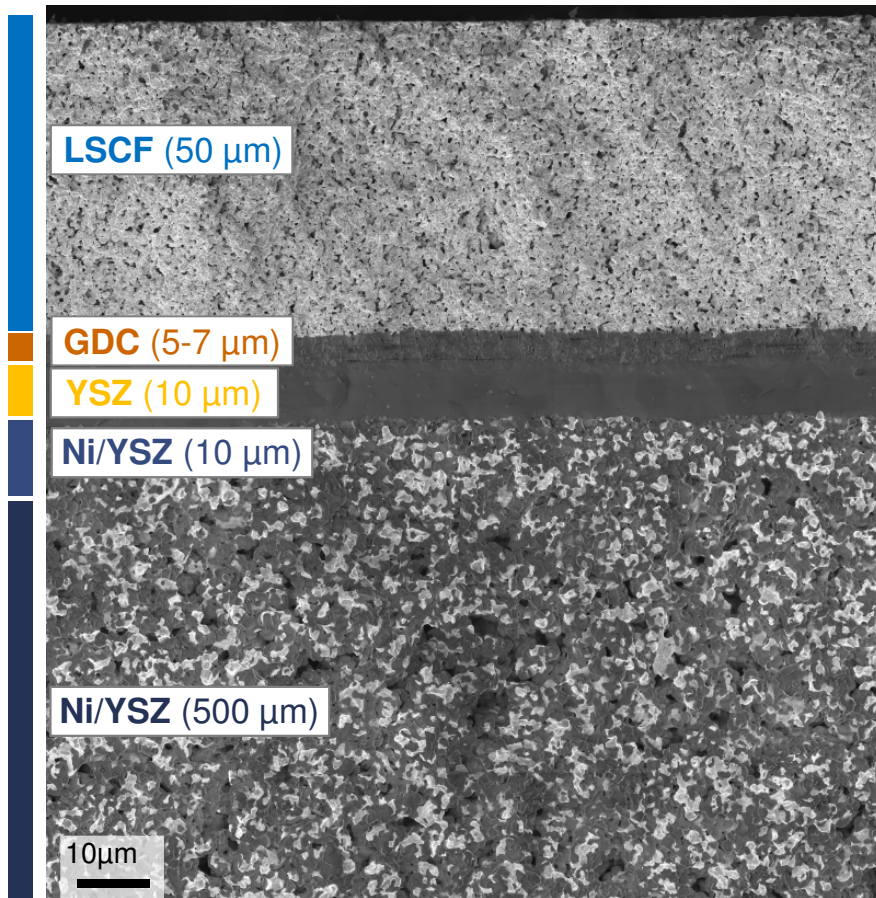
Formation and Degradation



Cathode/Electrolyte Interface



Cathode/Electrolyte Interface Distribution of Secondary Phases



Cathode
LSCF

Interlayer
GDC

SZO

ID

YSZ
Electrolyte
YSZ

Cathode/Electrolyte Interface Impact of Processing Conditions

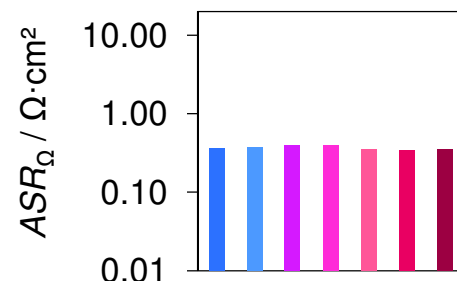
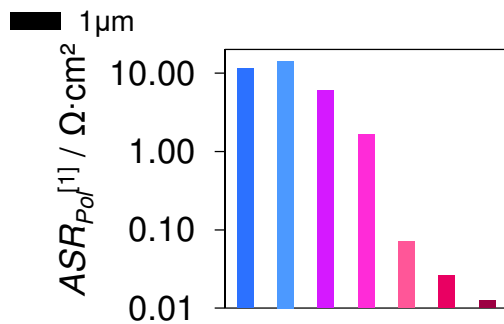
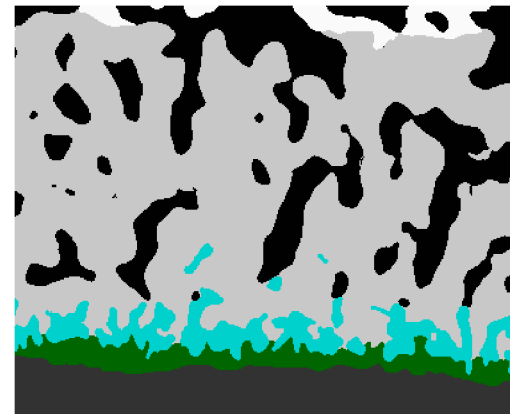
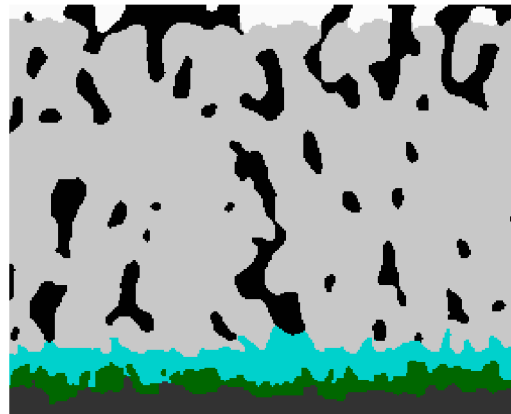
GDC sintering temperature

1100°C

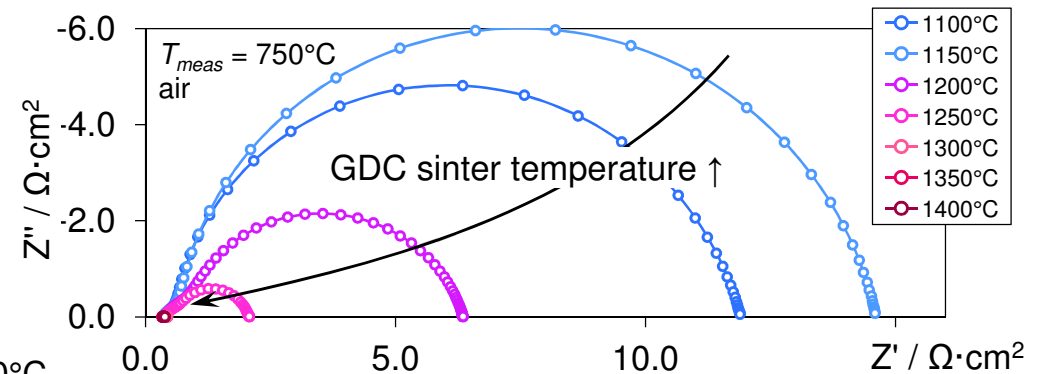
1200°C

1300°C

1400°C



1100°C 1150°C 1200°C 1250°C 1300°C 1350°C 1400°C

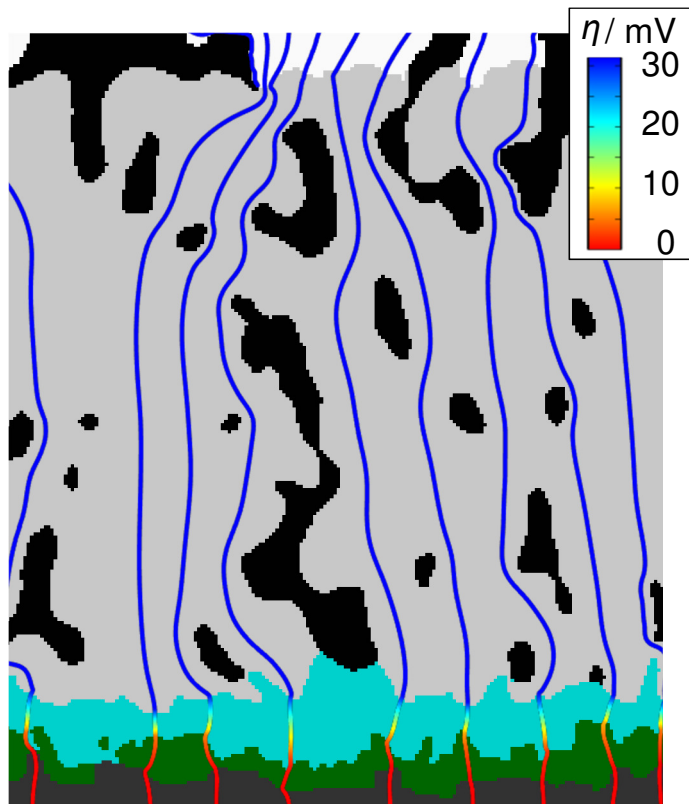


Cathode/Electrolyte Interface

Cathode Overpotential and Current Pathways

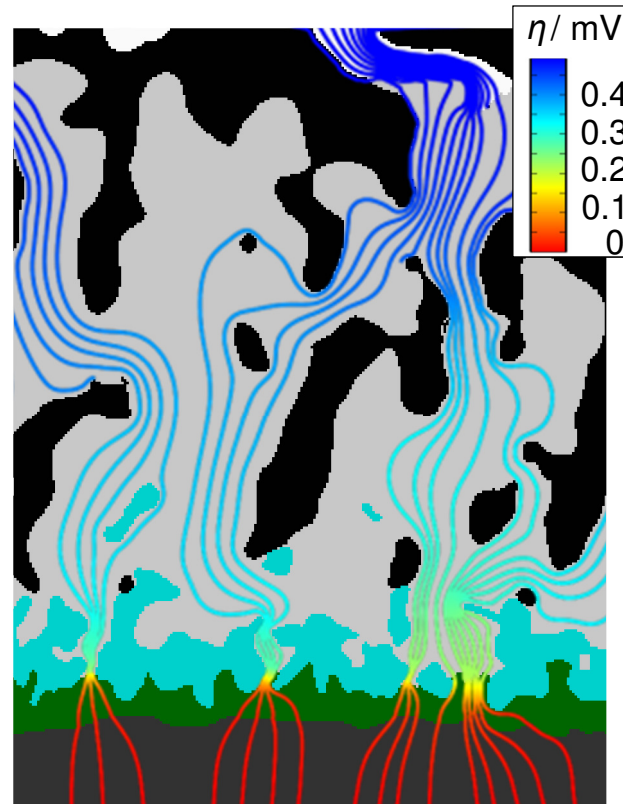
Continuous SrZrO_3

■ 1200°C



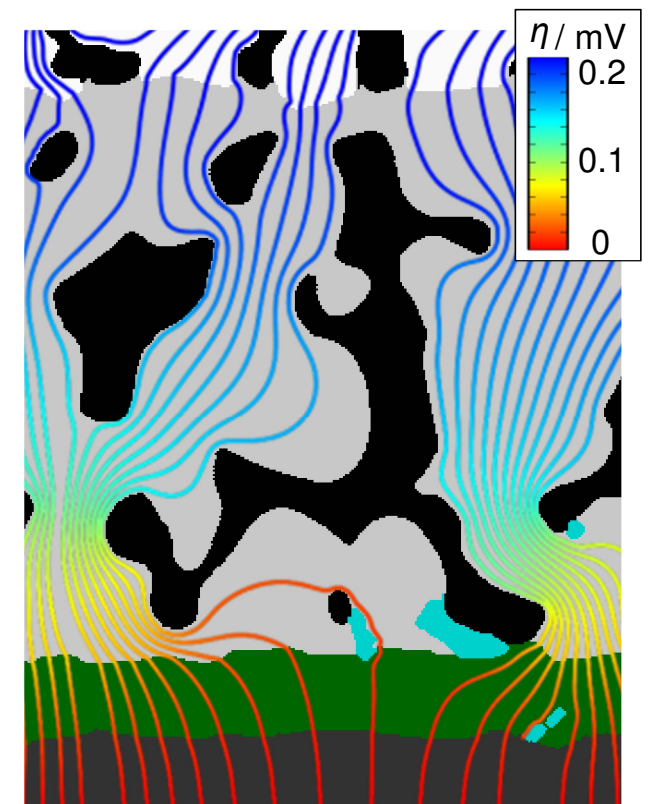
Intermittent SrZrO_3

■ 1300°C

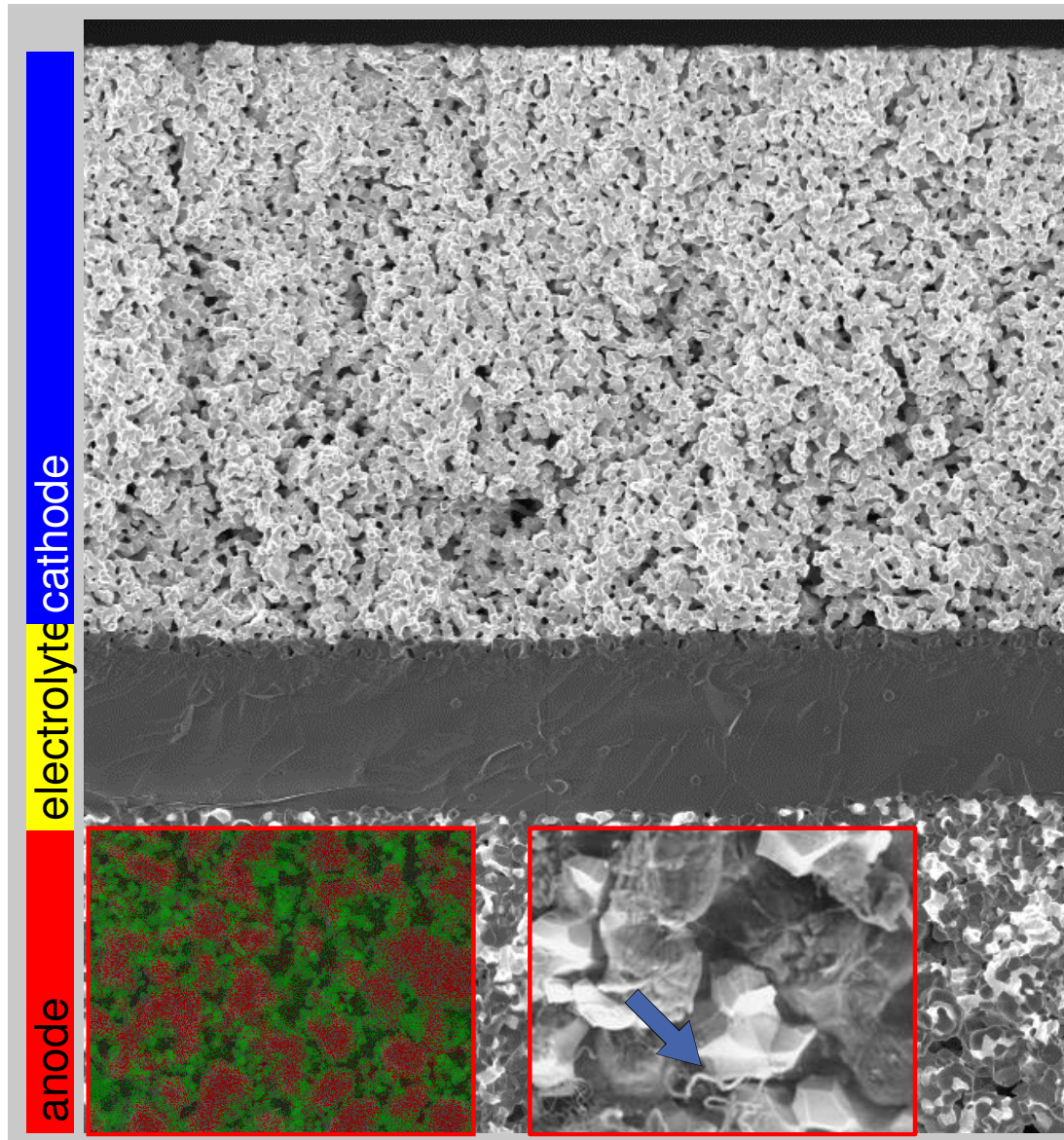


Continuous Interdiffusion

■ 1400°C



@ $f = 0.01 \text{ Hz}$ $j = 10 \text{ mA/cm}^2$ $T_{\text{meas}} \approx 800^\circ\text{C}$

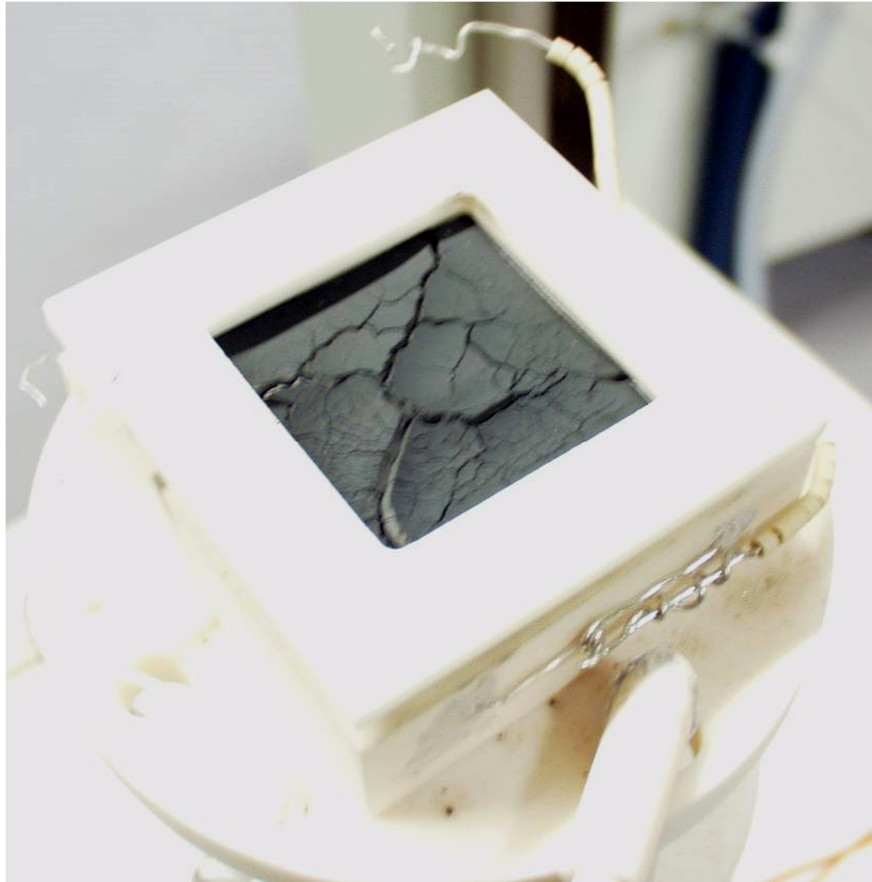


in **SOFC** many potentially competing degradation mechanisms are known:

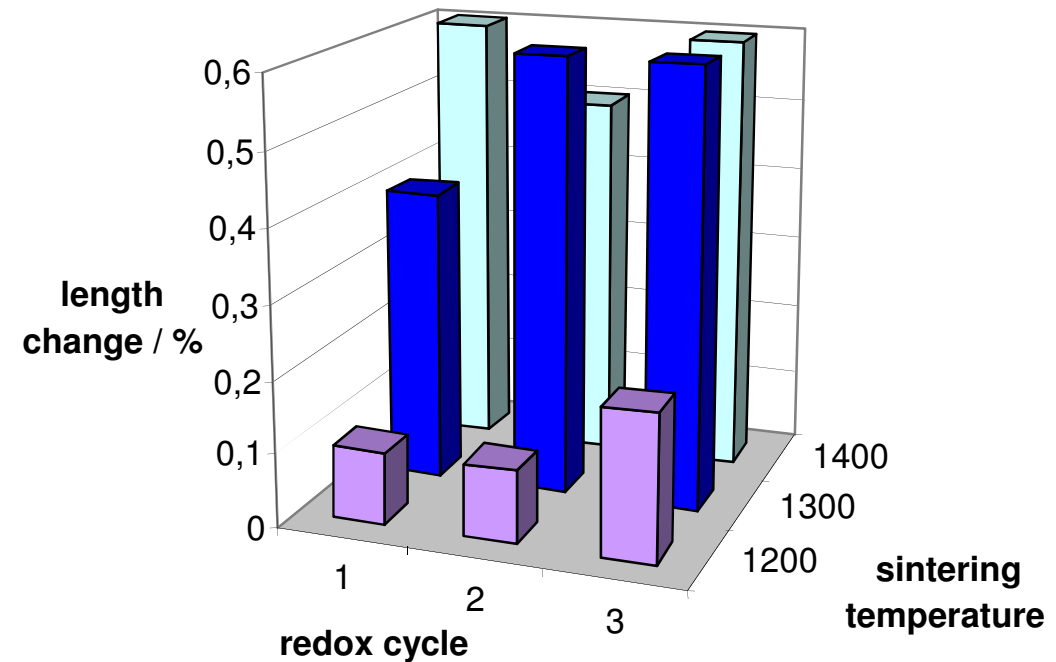
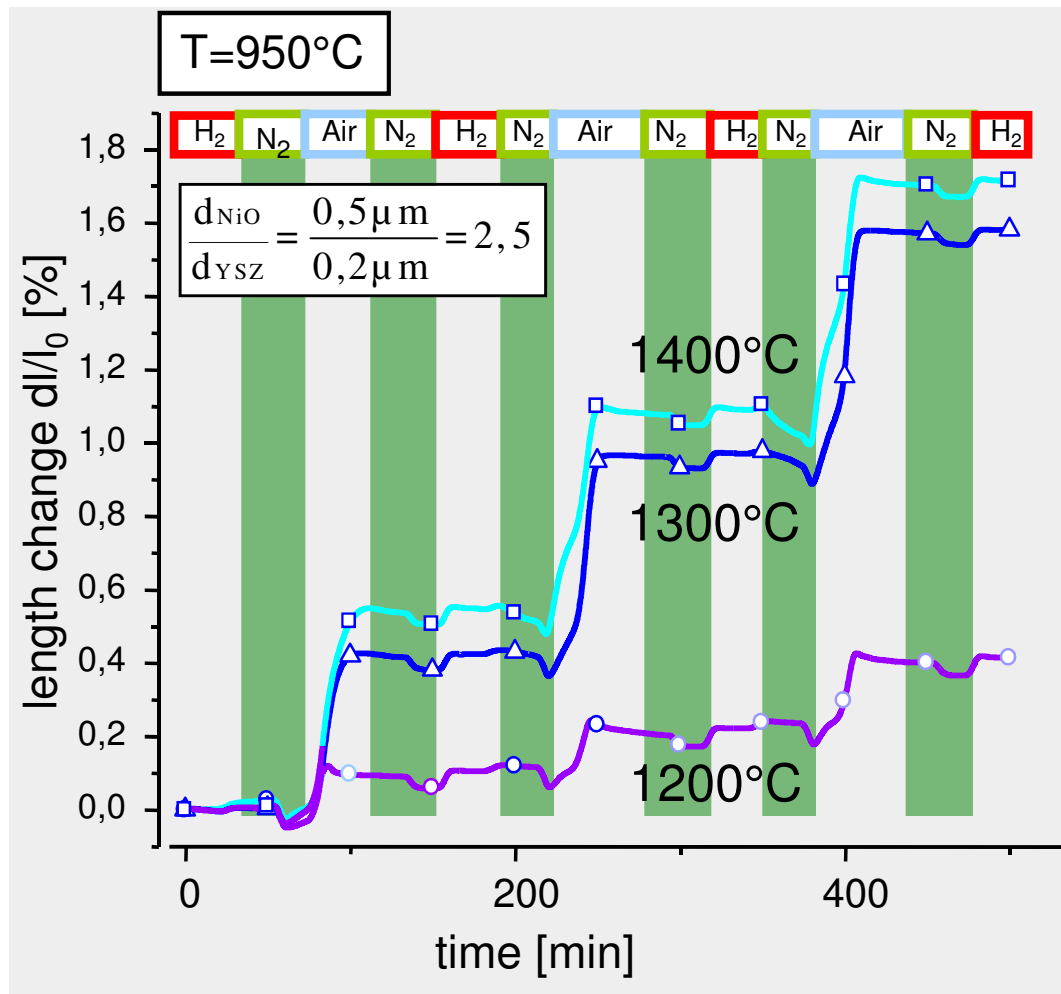
- Ni-agglomeration
A. C. Müller et. al., *Proc. 3rd European SOFC Forum*, pp. 353-362 (1998).
- carbon deposition
E. Ivers-Tiffée et. al., *Handbook of Fuel Cells – Fundamentals, Technology and Applications*, pp. 933-956 (2009).

Extrinsic Degradation

Cracking of an Anode Supported Electrolyte after Redox-Cycling



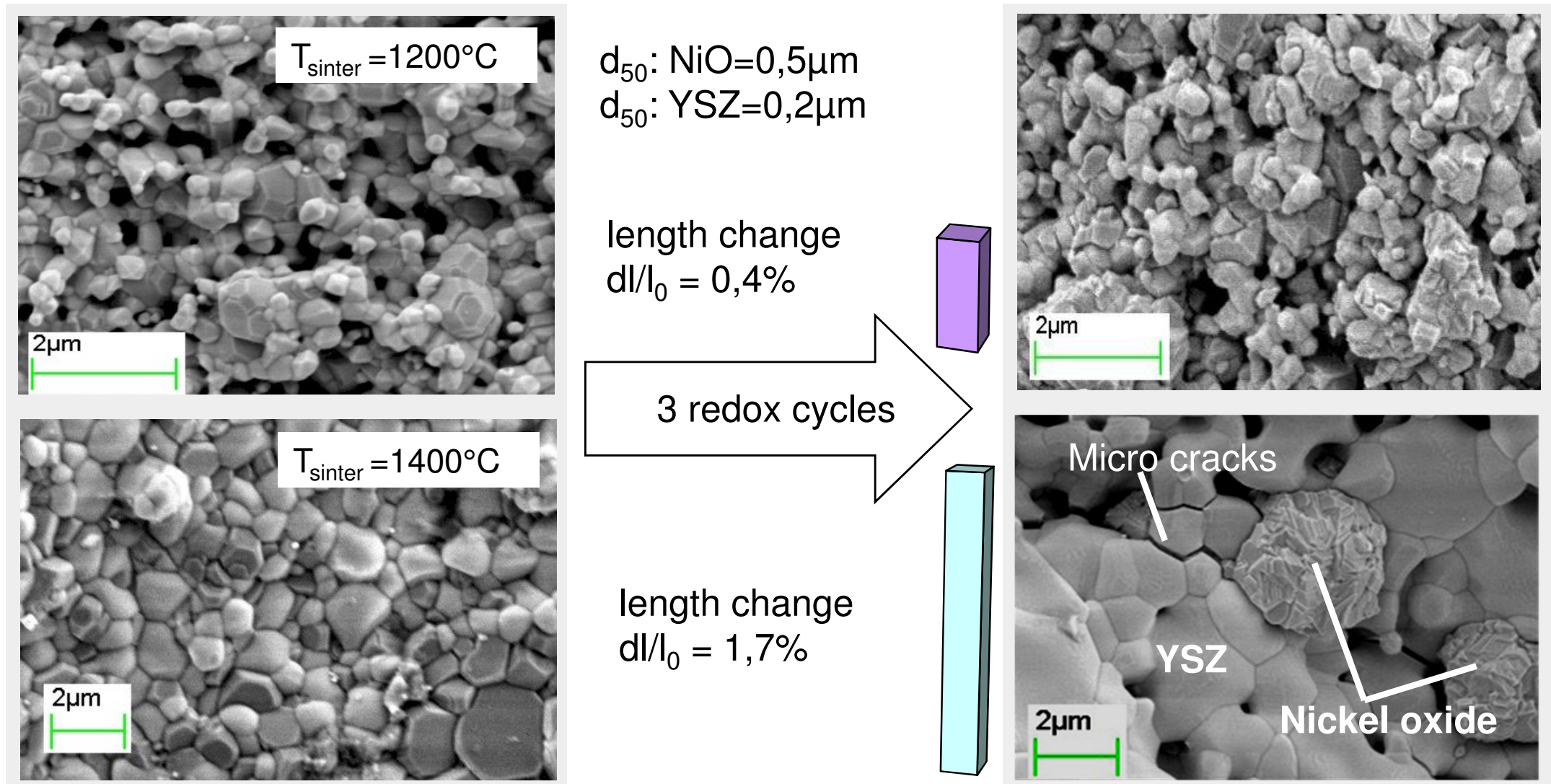
Impact of Redox Cycle on Length Change of Ni/YSZ Bulks: Different Sintering Temperatures



➤ minimum length change at lowest sintering temperature of 1200 °C

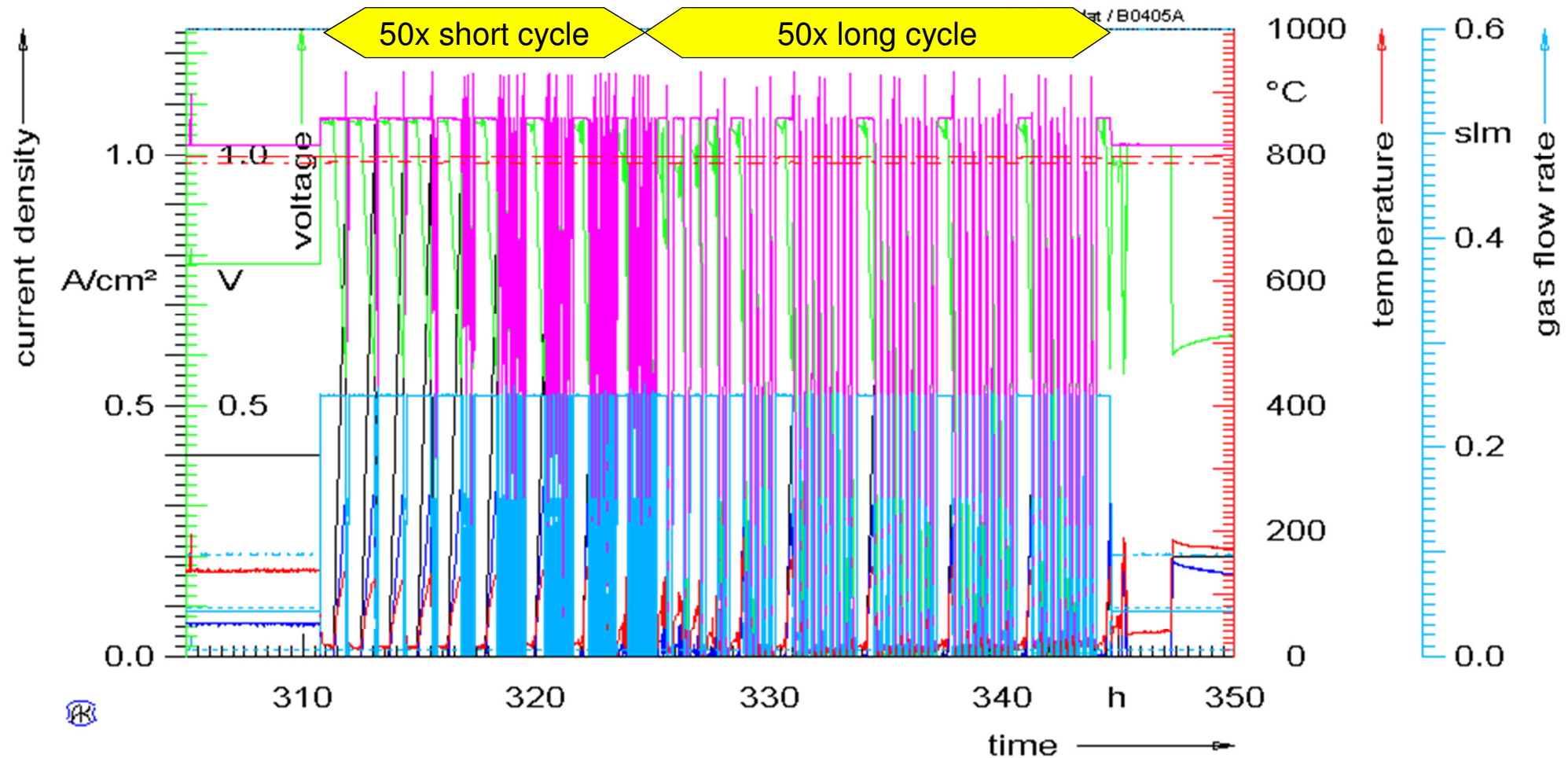
Impact of Redox Cycles on Microstructure of Ni/YSZ Bulks

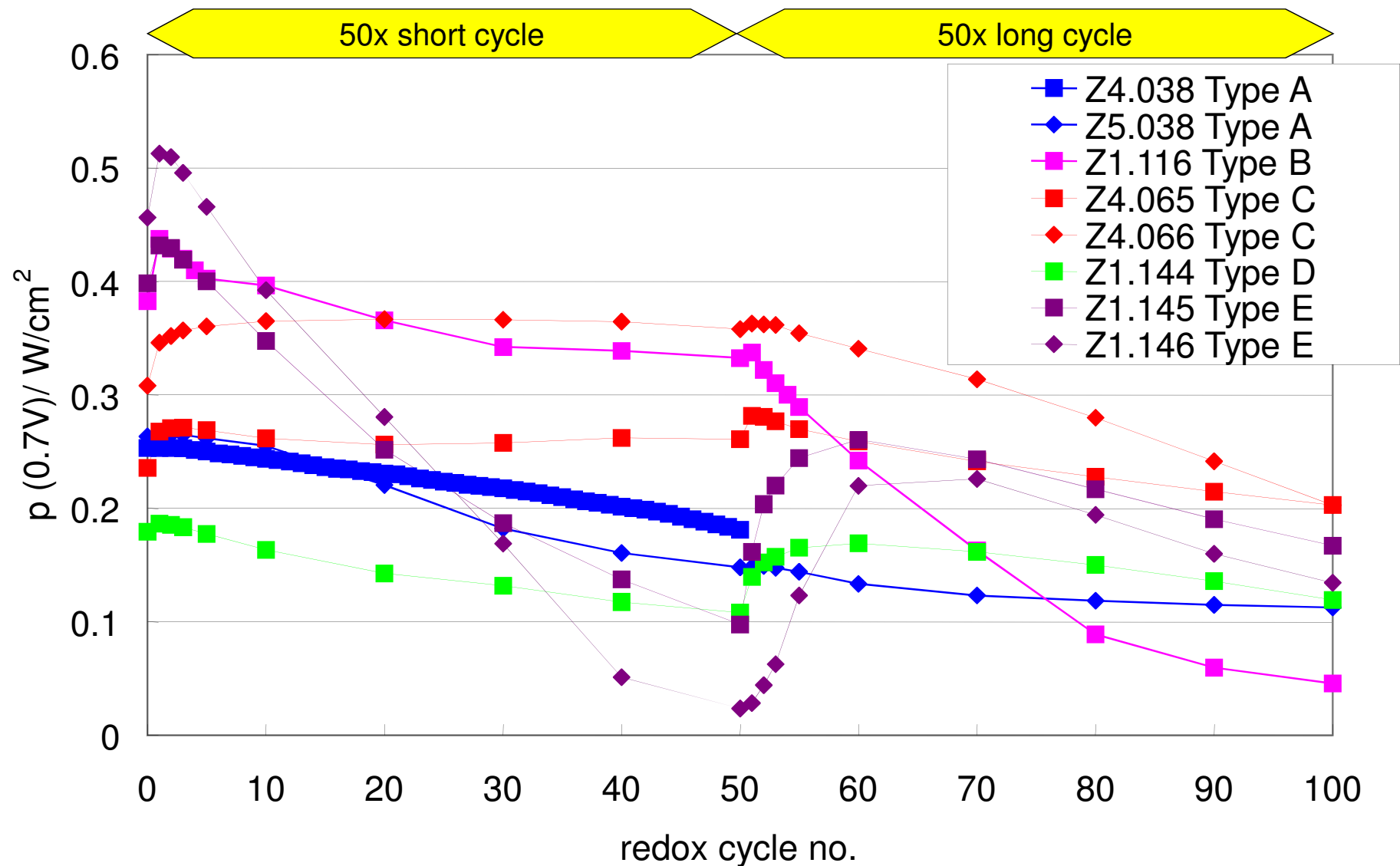
Different Sintering Temperatures



Degradation Tests for SOFC

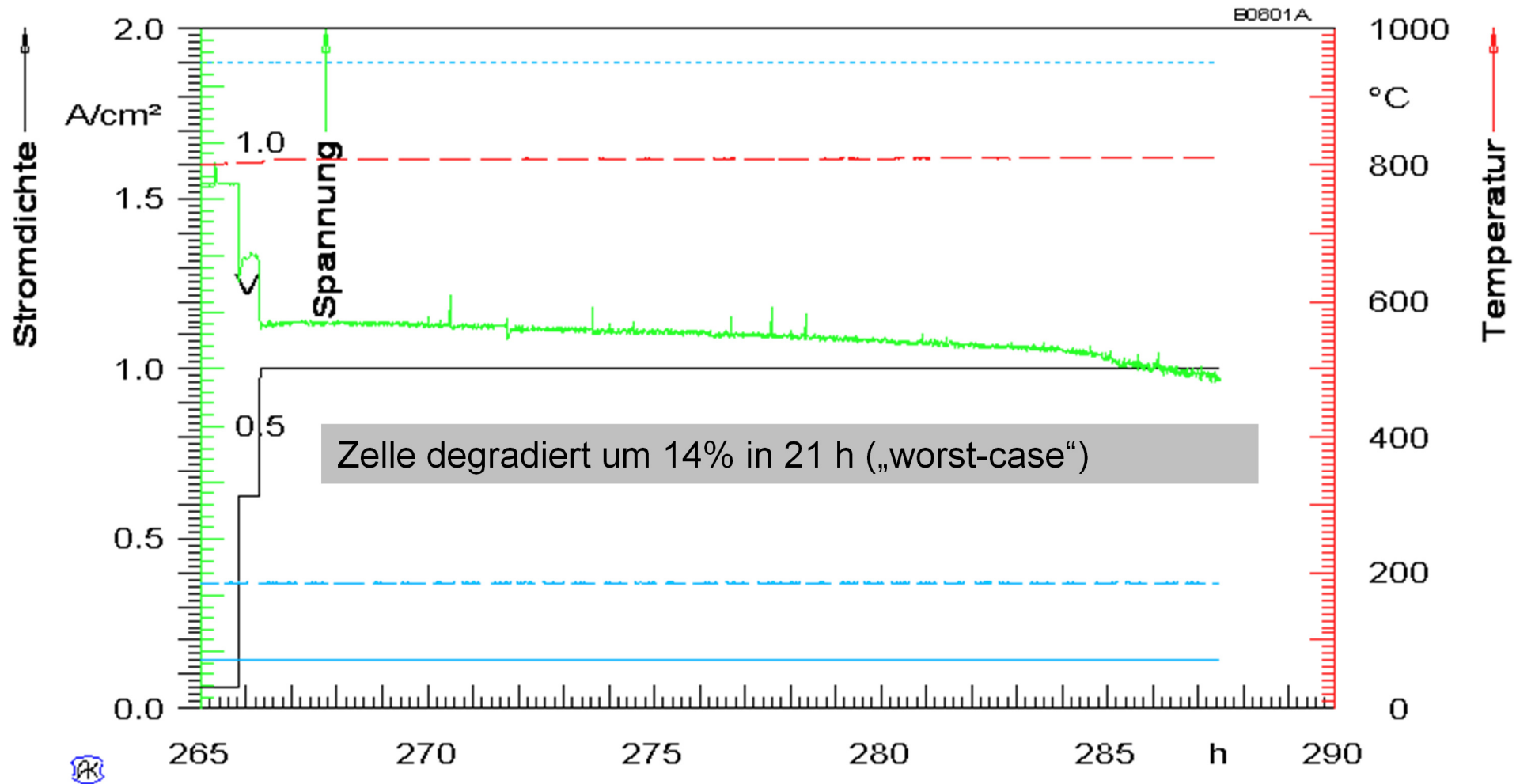
Redox Stability (100 Redox-Cycles in 35 h)





Operation on Hydrocarbons

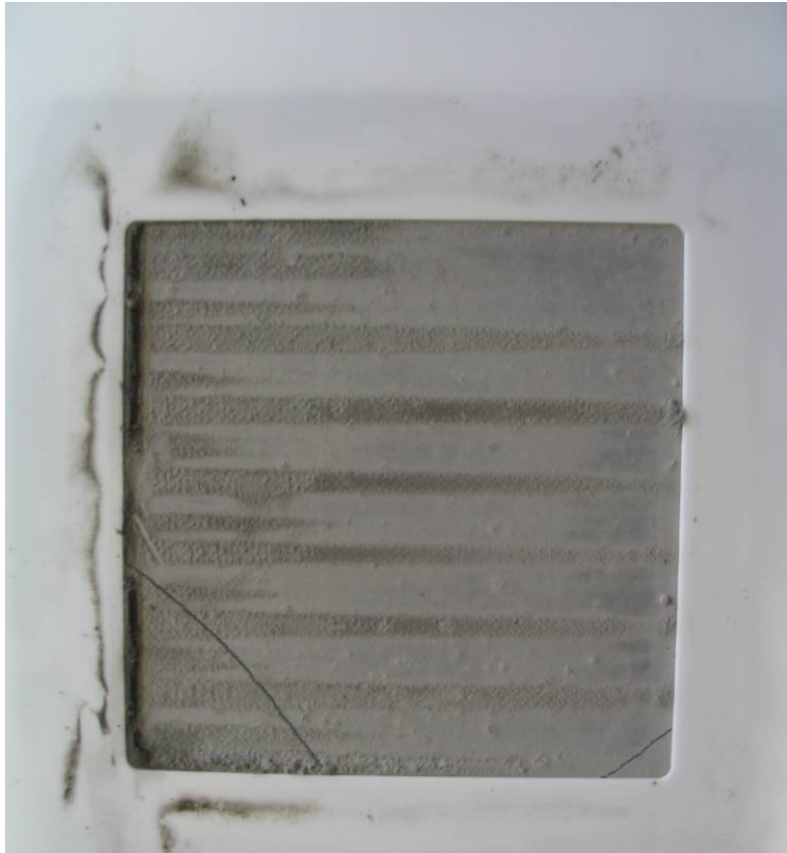
Severe Degradation with higher Hydrocarbons C_nH_m



Gasgemisch: H_2 , CO , H_2O , CO_2 , N_2 , C_2H_2 (Ethin), C_7H_8 (Toluol), Methylnaphtalin ($C_{11}H_{10}$)

Operation on Hydrocarbons

Severe Degradation with higher Hydrocarbons C_nH_m

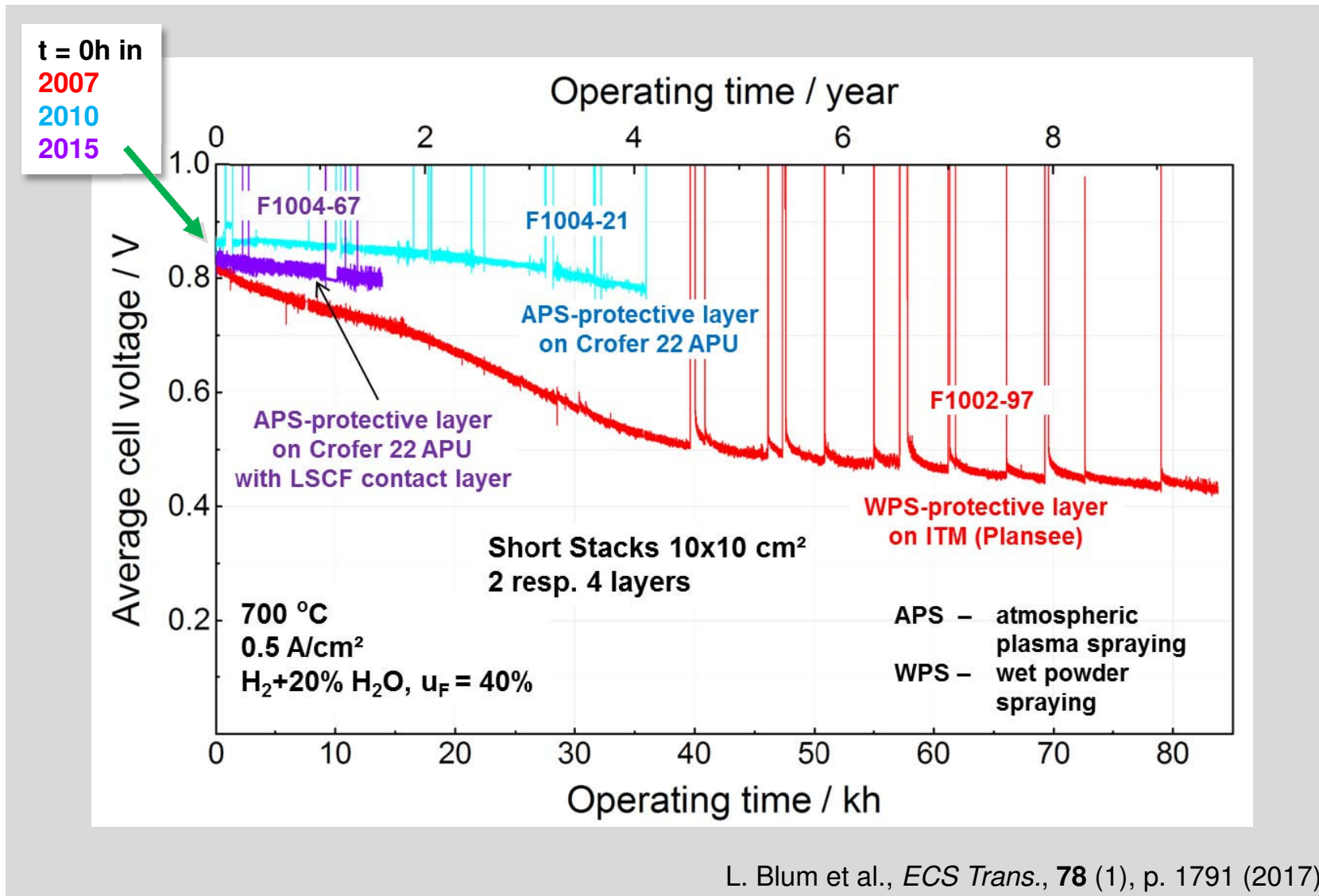


Aufgekohlte Zelle nach Betrieb mit einem Gasgemisch bestehend aus H_2 , CO , H_2O , CO_2 , N_2 , C_2H_2 (Ethin), C_7H_8 (Toluol) und Methylnaphtalin ($C_{11}H_{10}$)

→
Flussrichtung

Durability Testing of Solid Oxide Cells

Research Center Jülich ASC-Stacks (2007 ff)



duration

> 80 000 h
~ 10 years
2007 – today

degradation

0.3 ... 0.6 % /
1 000 h

results

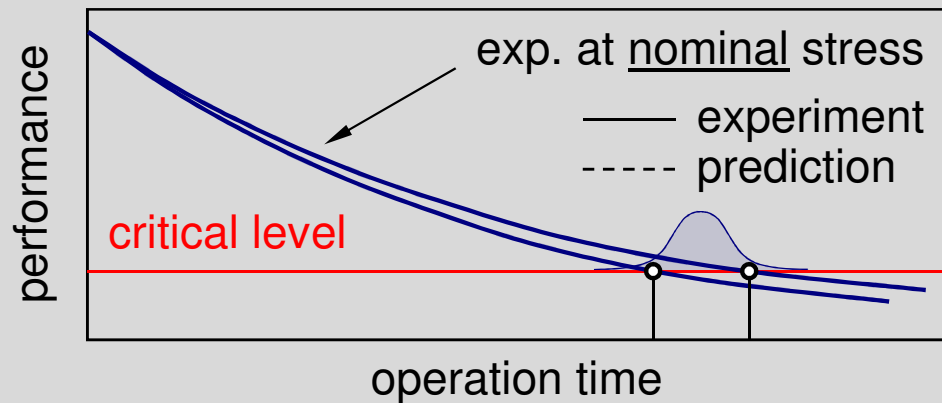
available after
5...10 years



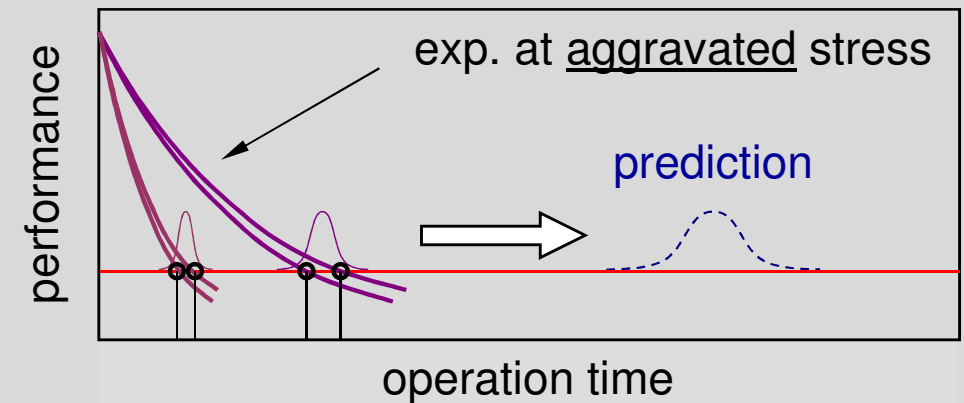
**accelerate
testing !**

Accelerated Testing

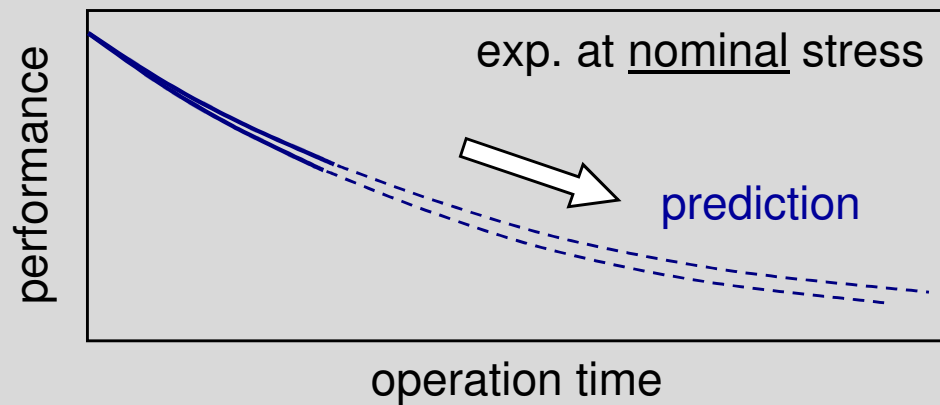
"conventional" life testing



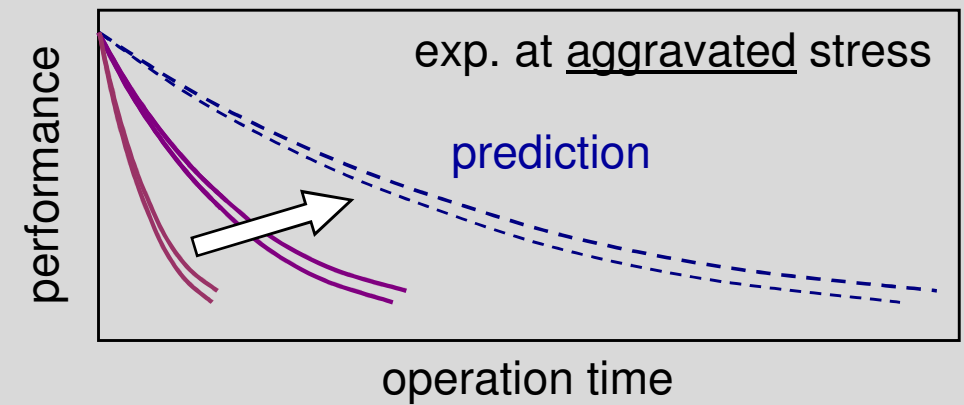
accelerated life testing



degradation testing



accelerated degradation testing



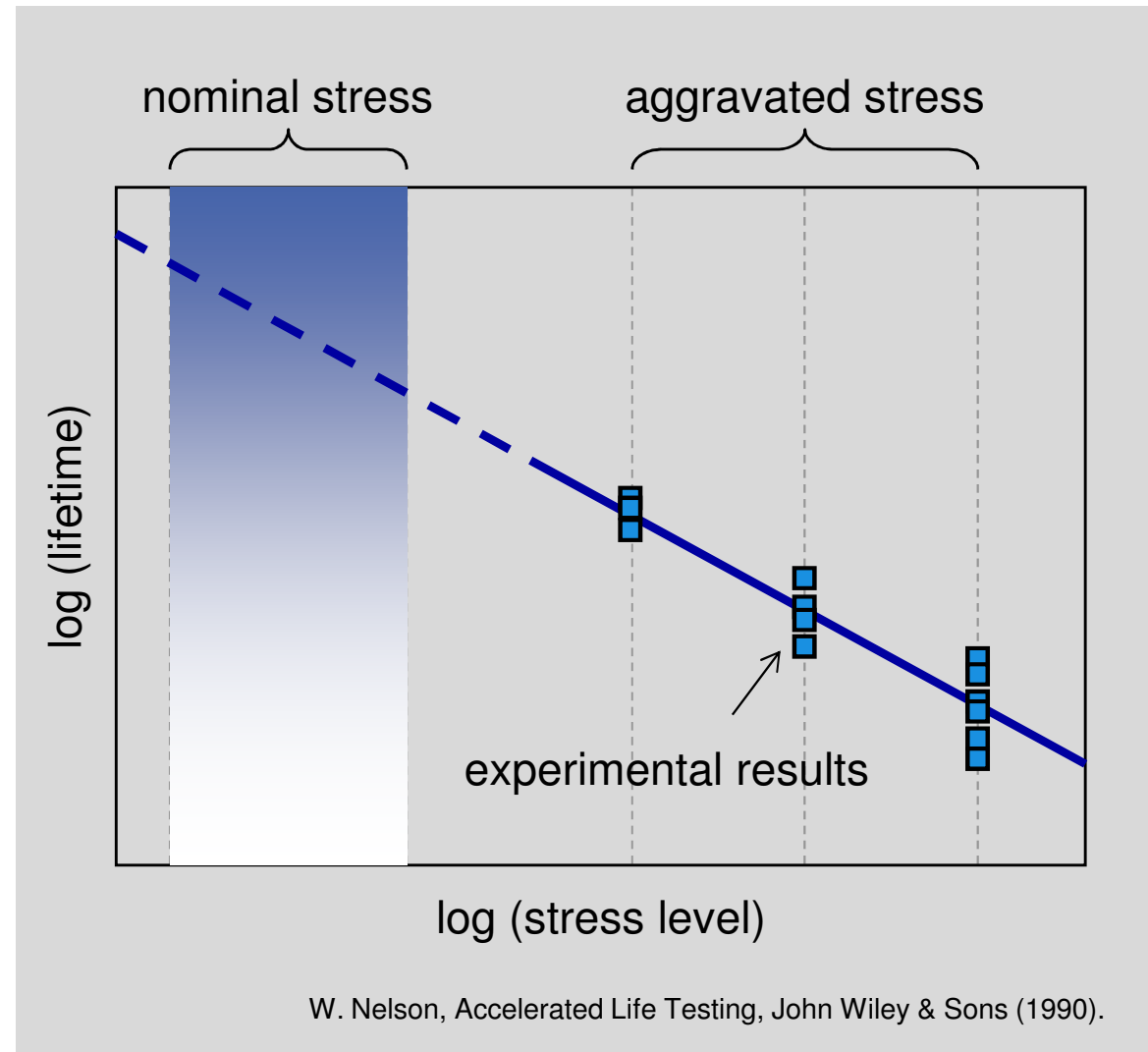
Accelerated Testing Approach and Advantages

approach

- degradation is accelerated by means of aggravated stress (current load, temperature, etc.).
- life-stress relationship is modelled by the use of failure data.
- extrapolation of life-stress model gives a prediction for service life at nominal stress.

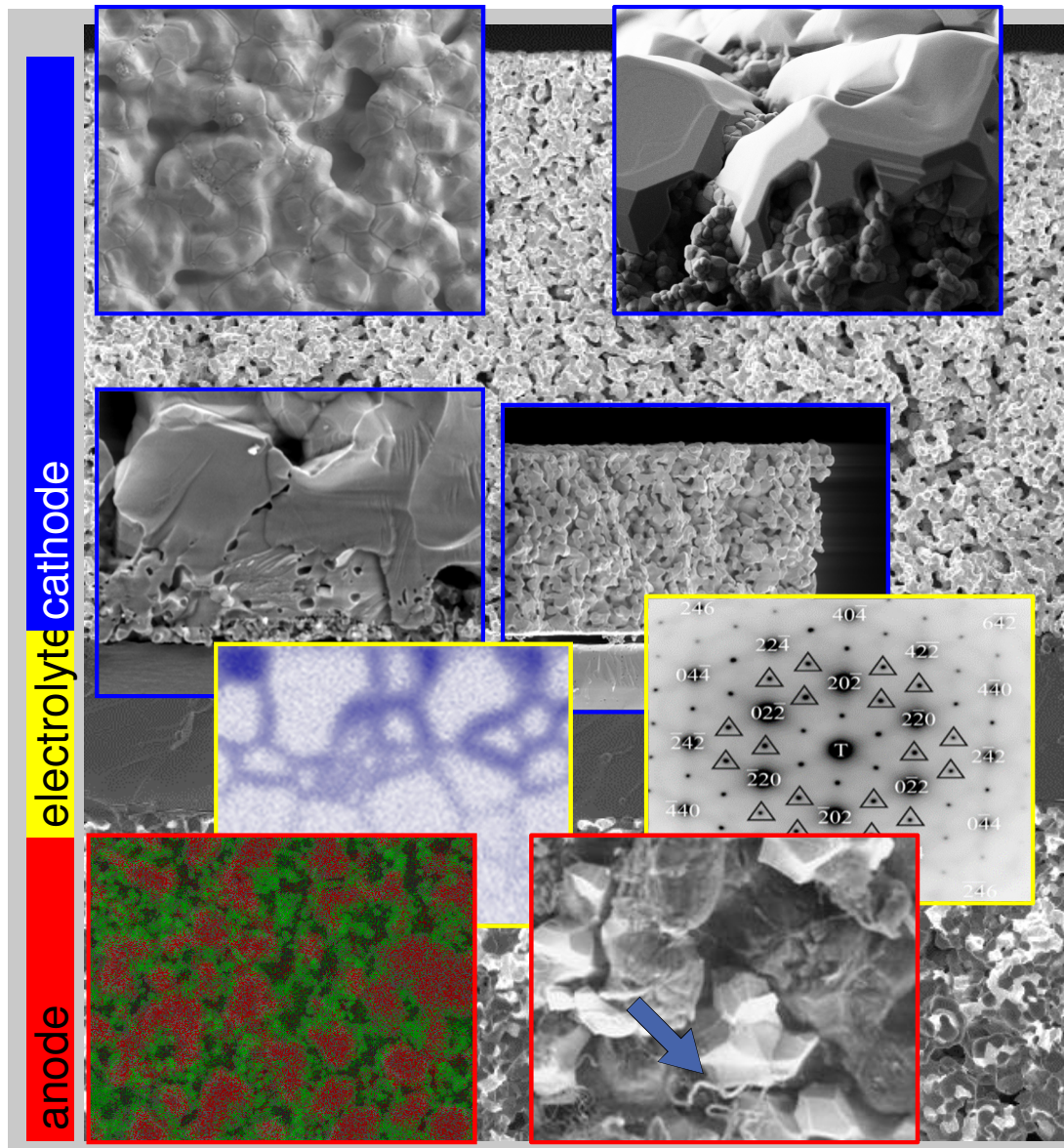
advantages of ALT

- physical consequences of degradation appear more clearly, mechanisms are identified more easily.
- precious measurement time is saved, lifetime is evaluated rapidly.



Accelerated Life Testing

Competing Degradation Processes in Solid Oxide Cells



in **SOC** many potentially competing degradation mechanisms are known:

- densification of electrodes
A. Weber et. al., *Denki Kagaku* **64**, pp. 582-589 (1996).
 - formation of micropores
 - formation of chromium compounds on the cathode
 - delamination of the cathode
M. J. Heneka et. al., *Proc. 9th Int. Symp. on SOFC*, pp. 534-543 (2005).
 - Mn-interdiffusion
A. Weber, in J. Garche (Ed.), *Encyclopedia of Electrochemical Power Sources*, Amsterdam: Elsevier, pp. 120-134 (2009).
 - intrinsic electrolyte degradation
B. Butz et. al., *Solid State Ionics* **177**, pp. 3275-3284 (2006).
 - Ni-agglomeration
A. C. Müller et. al., *Proc. 3rd European SOFC Forum*, pp. 353-362 (1998).
 - carbon deposition
E. Ivers-Tiffée et. al., *Handbook of Fuel Cells – Fundamentals, Technology and Applications*, pp. 933-956 (2009).
- ⇒ in addition, activation processes that improve the performance take place
A. Weber et. al., *Denki Kagaku* **64**, pp. 582-589 (1996).

Accelerated Life Testing

Competing Degradation Processes

aging mechanism A

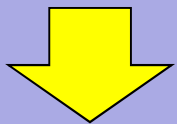
- experimental results
- life-stress model
- - extrapolation

aging mechanism B

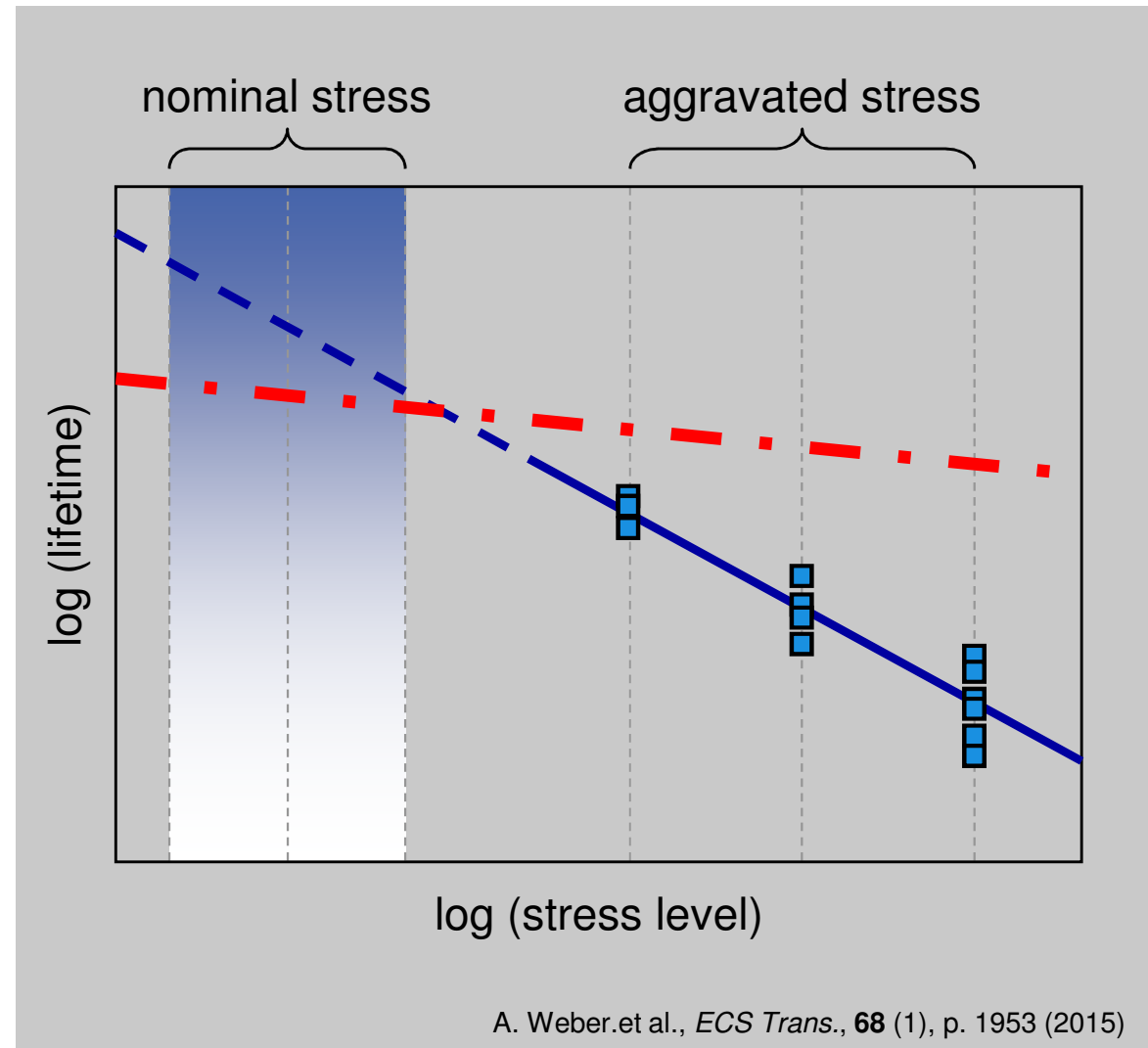
- - different life-stress dependency

aging mechanism B

- different dependency on stress level
- minor impact at aggravated stress
- lifetime limiting at nominal stress



ALT approach will fail



Degradation Testing

Deconvolution of Competing Degradation Processes

aging mechanism A

- experimental results
- life-stress model
- - extrapolation

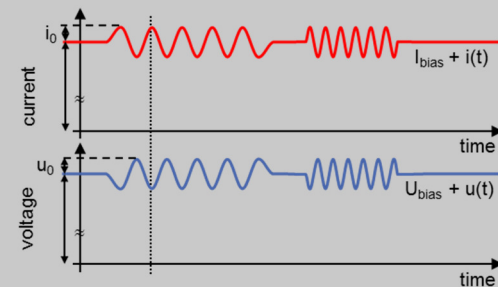
aging mechanism B

- · different life-stress dependency

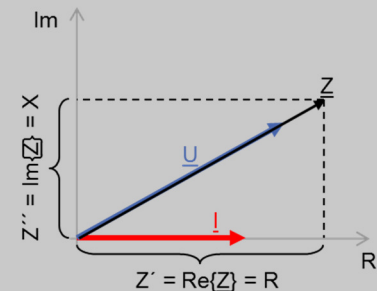
→ **deconvolute aging mechanisms**

- ~~overall performance, lifetime~~
~~(summarized / averaged quantities)~~
- physicochemical processes acquired via their electrochemical impedance (additive quantities)

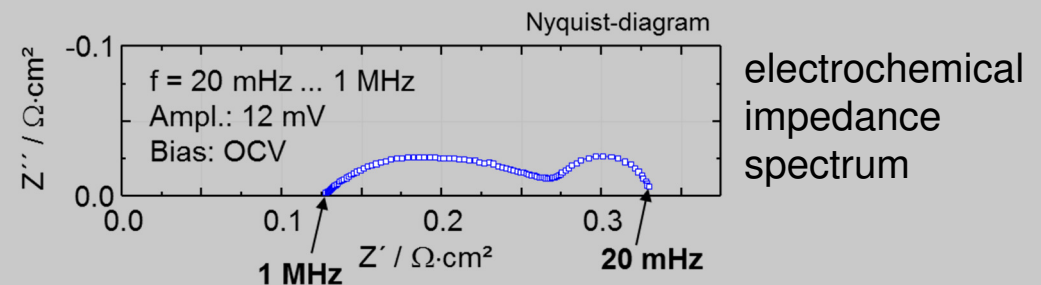
EIS: electrochemical impedance spectroscopy



- sinusoidal electrical stimulation (current)
- linear regime → small amplitude
- sinusoidal electrical response (voltage)



- variation of the stimulation frequency → processes in the cell with a lower relaxation frequency are not stimulated



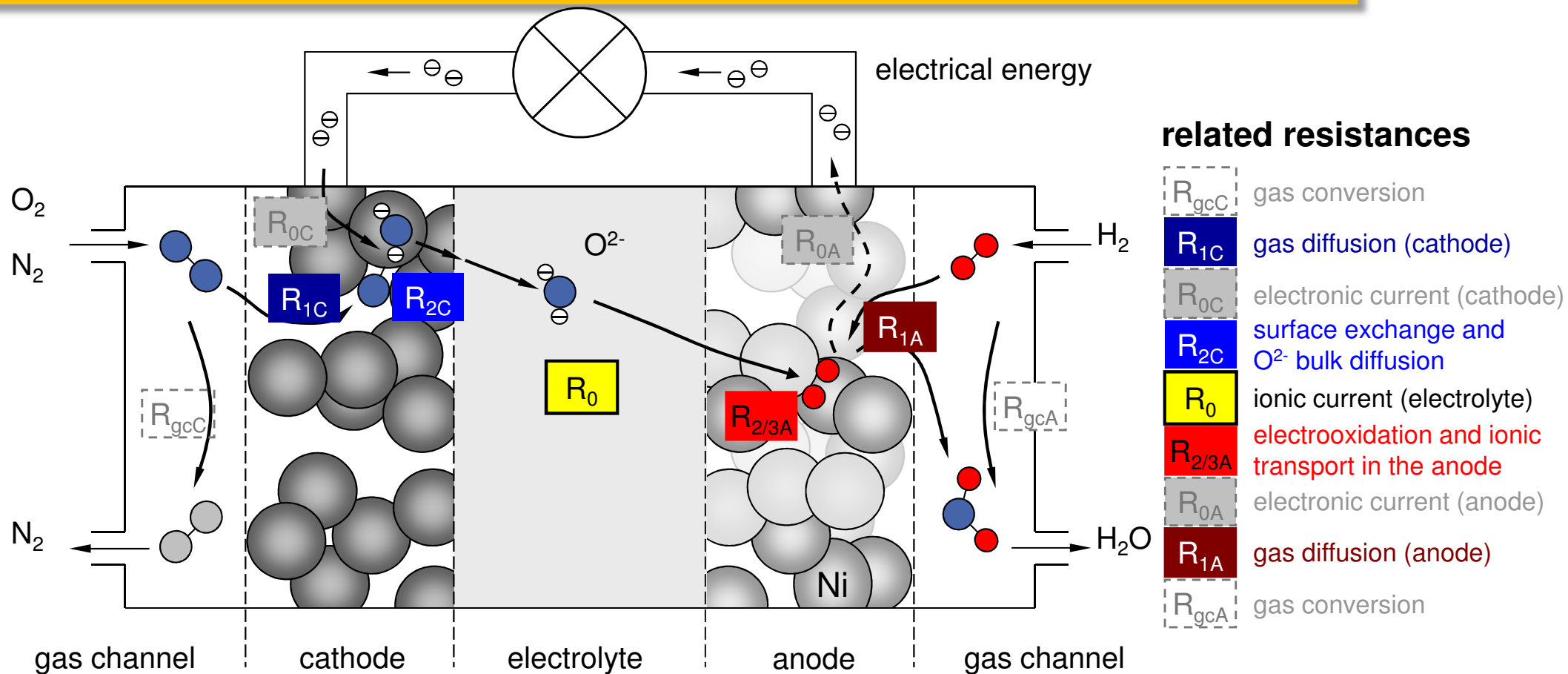
Loss mechanisms in SOFCs

Processes contributing to the Area Specific Resistance (ASR)

Transport in the gas phase: gas flow and diffusion

Transport in the solid phase: electronic and ionic current

Reactions: charge transfer, surface exchange, electrooxidation, surface catalysis

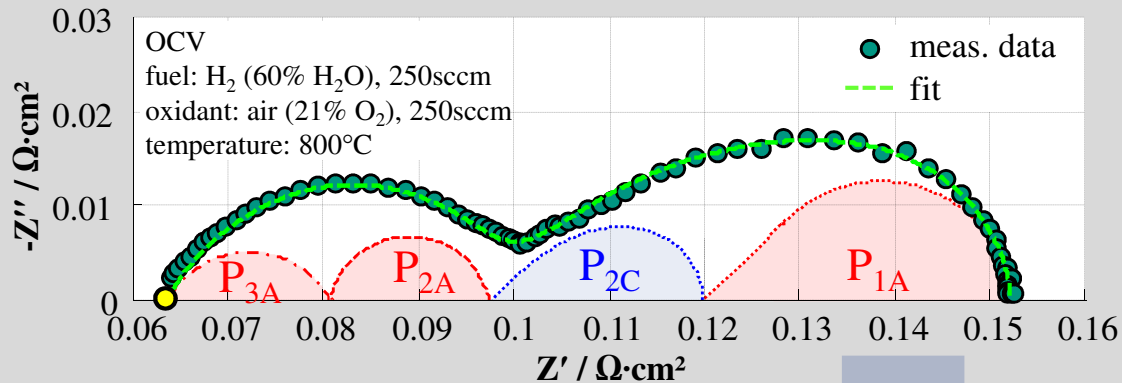


Impedance based Cell Model I

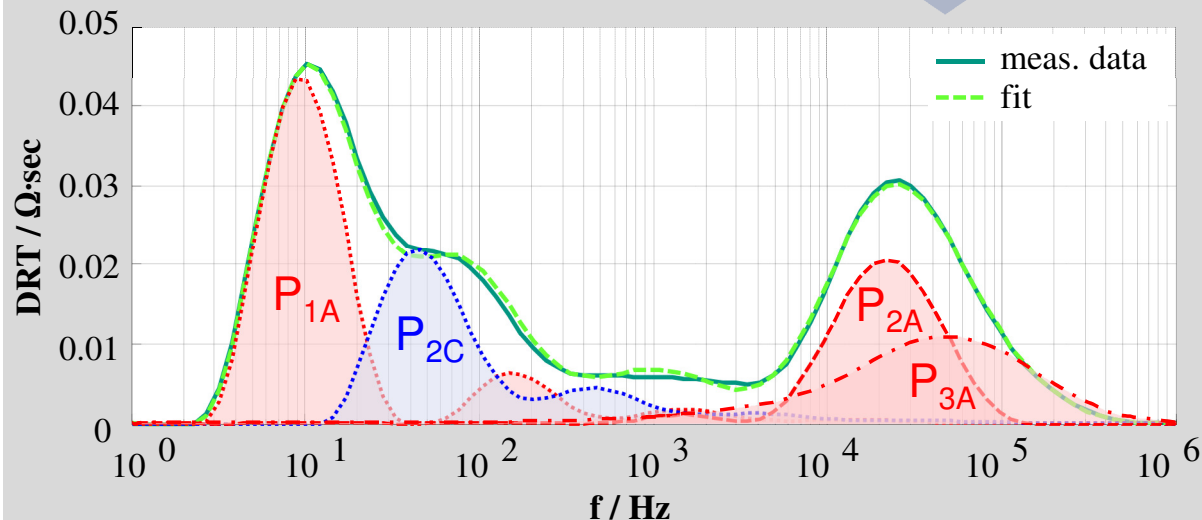
Deconvolution of electrochemical Processes

Electrochemical Impedance Spectroscopy EIS

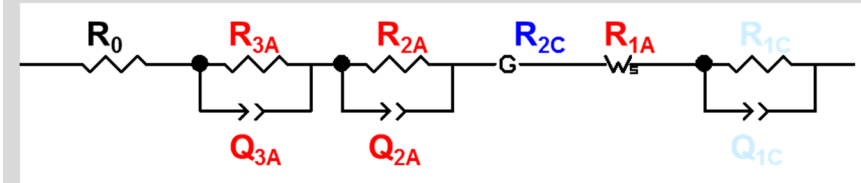
ASC: Anode-Supported Cell
OCV: Open Circuit Voltage



Distribution of Relaxation Times DRT $Z(\omega) = R_{Pol} \int_0^\infty \frac{\gamma(\tau)}{1+j\omega\tau} d\tau$



equivalent circuit model



process	physicochemical origin
P _{1C}	gas diffusion (cathode)
P _{2C}	oxygen reduction reaction (cathode)
R ₀	ionic (and electronic) conduction
P _{2A} / P _{3A}	hydrogen electrooxidation coupled with gas diffusion and ionic transport
P _{1A}	gas diffusion (porous substrate)

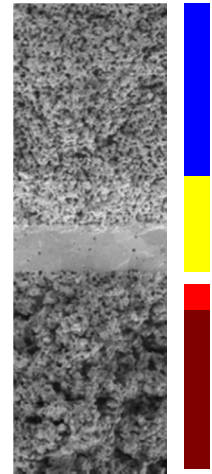


Model Application

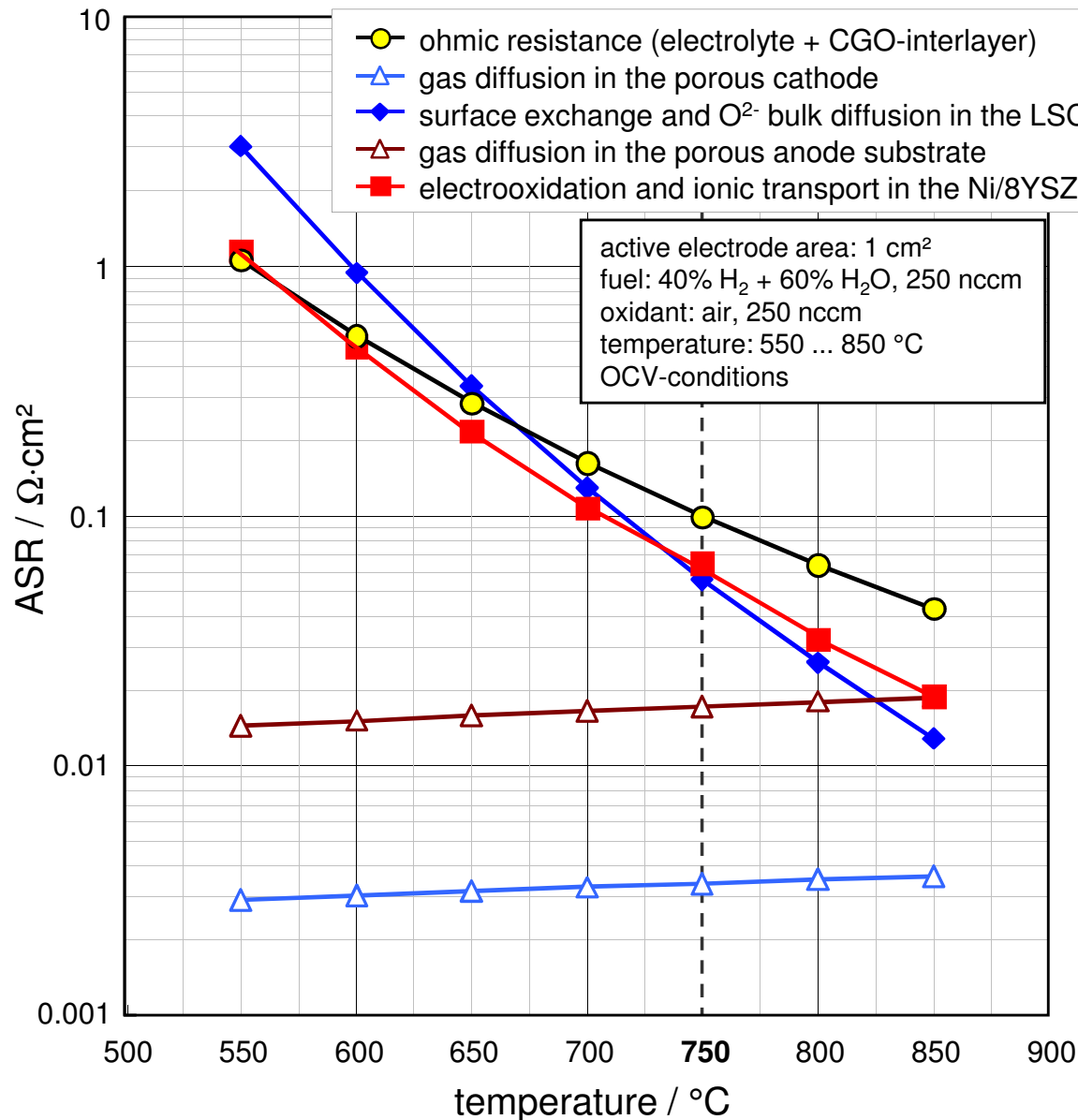
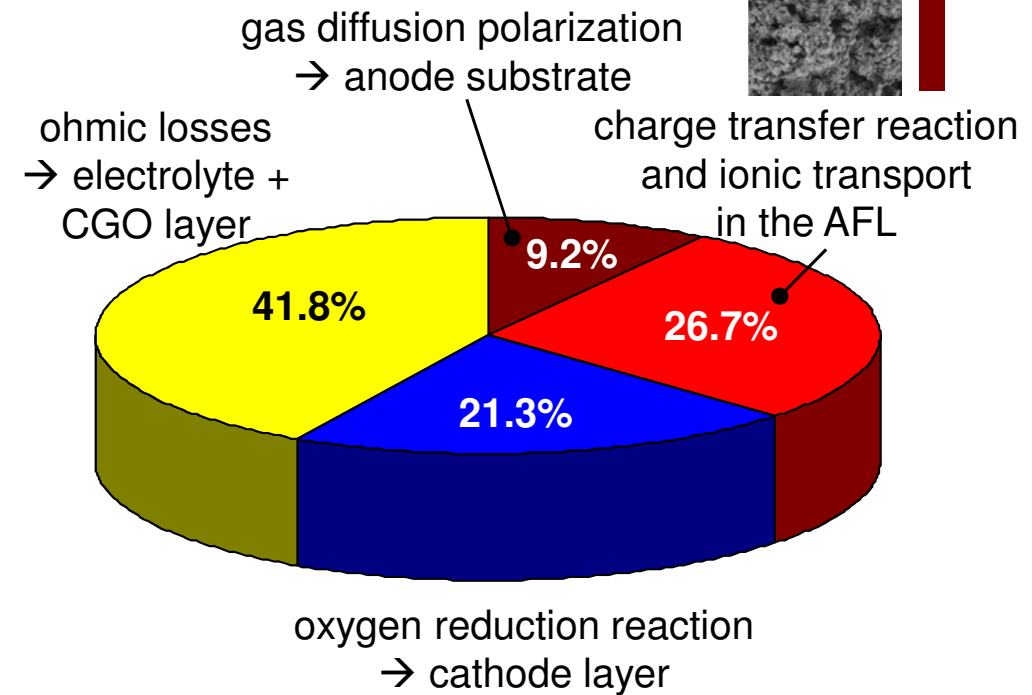
ASRs of the Cell Components



FZ Jülich ASC

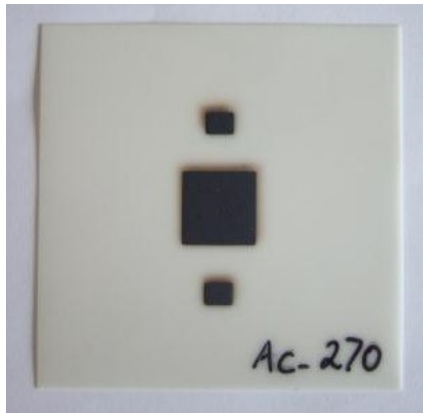


at 750 °C:



Applicability of the Model to different Cell Types

Cell Types analyzed in National and European Projects

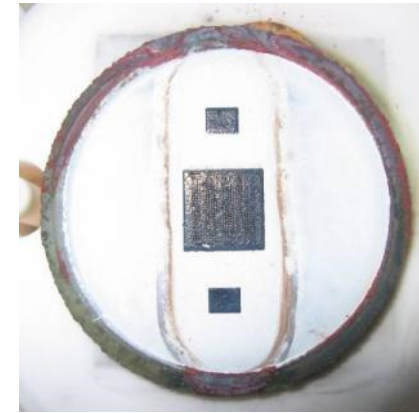


ESC

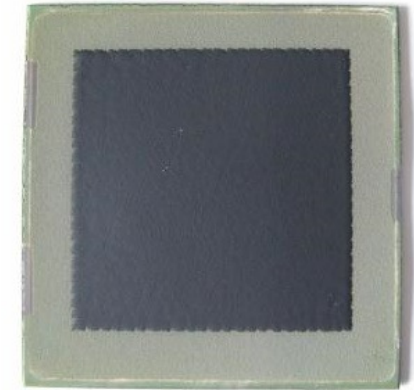
H.C.Starck 



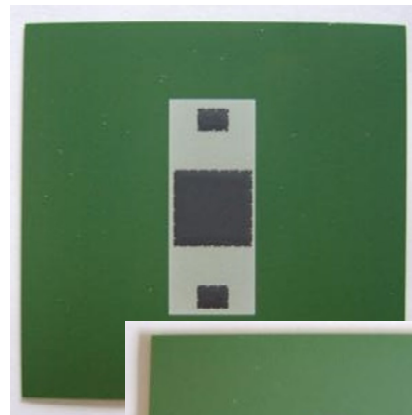
SrTiO₃-based ASC



 VPS-MSC

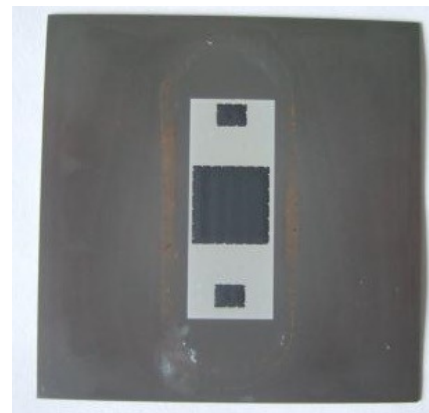


 APS-MSC
UNIVERSITY WEST



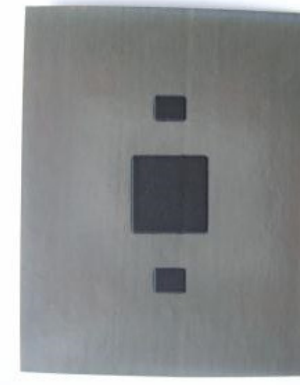

CeramTec
THE CERAMIC EXPERTS

SOLID
POWER

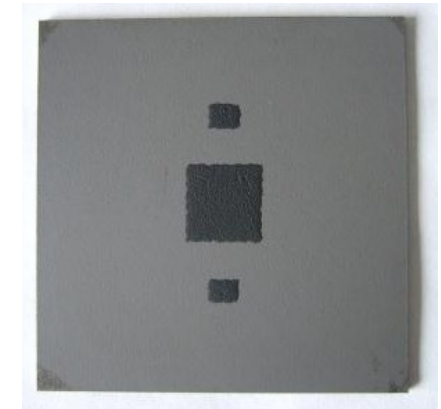


ASC (reduced)


TOPSOE FUEL CELL
clean, efficient and reliable



cofired MSC



 PVD MSC

ASC's (before reduction)

C. Endler-Schuck et al., *J. FC Science and Technology* **8**, p. 41001 (2011)
Q. Ma et al., *J. Power Sources* **196**, p. 7308 (2011)
P. Blennow et al., *J. Power Sources* **196**, p. 7117 (2011)
F. Han et al., *J. Power Sources* **218**, p. 157 (2012)
T. Franco et al., *Proc. 10th Eur. SOFC Forum*, p. A0906 (2012)
A. Kromp et al., *Fuel Cells* **13**, p. 598 (2013)

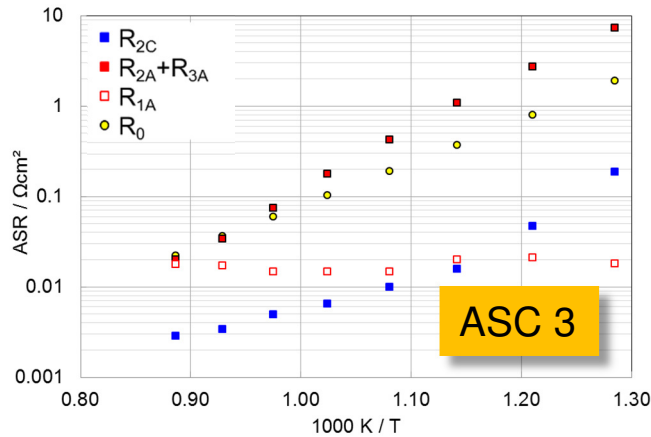
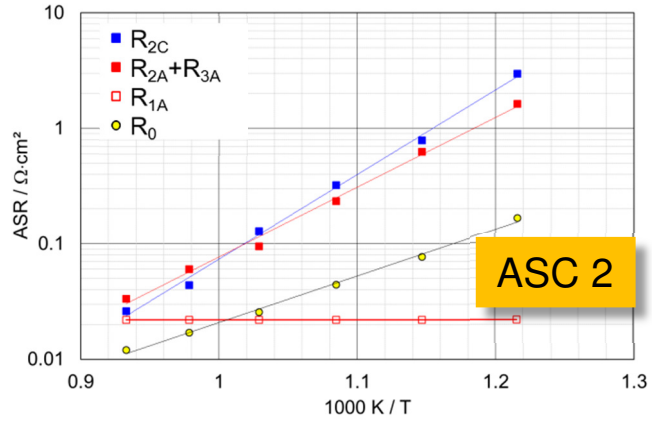
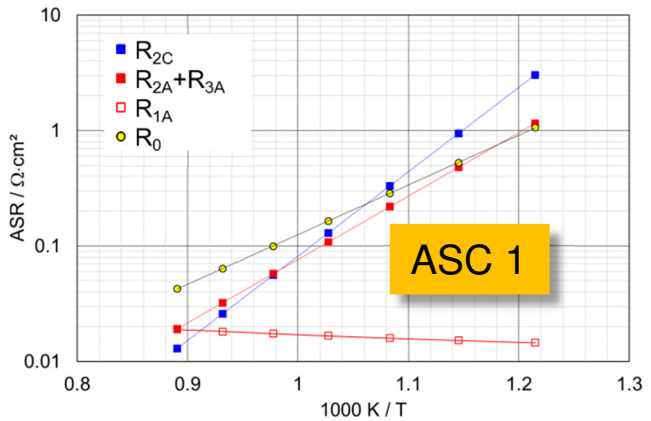

DTU


PLANSEE

www.iam.kit.edu/net



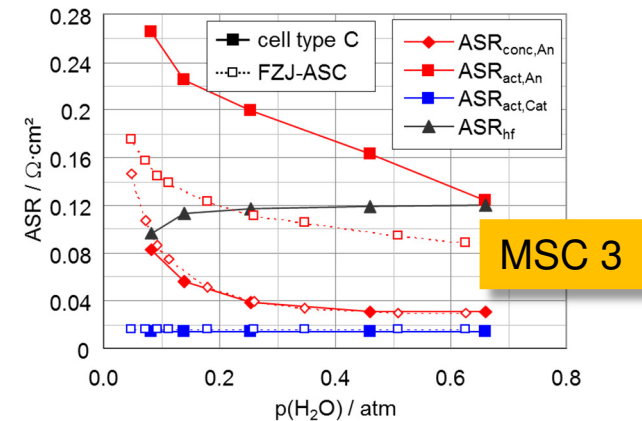
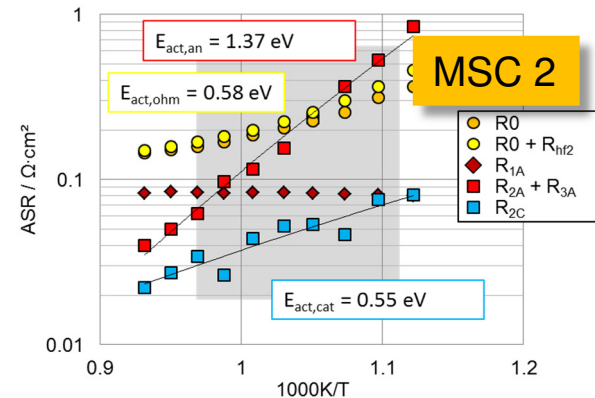
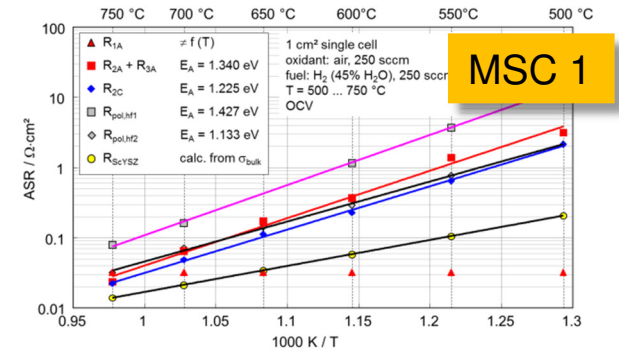
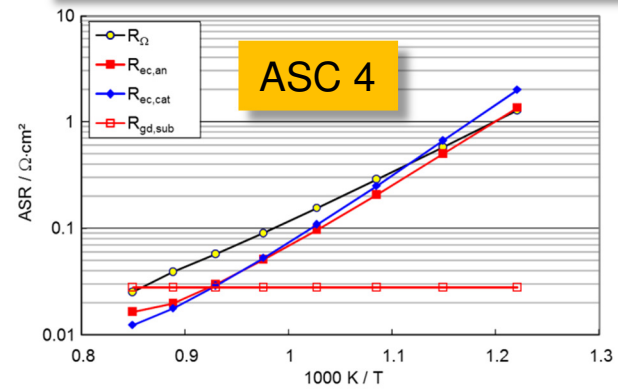
Applicability of the Model to different Cell Types



quite similar processes in all cells

- gas diffusion in the pores
- electronic / ionic currents in solids
- a MIEC-cathode
- a cermet anode

+ polarization at insulating interlayers



Impedance based Cell Model II

Physicochemical Performance Model → Power Density

model equations with 13 parameters from EIS

Nernst equation U_{OCV}

$$\text{ohmic loss } R_{ohm} = \frac{T}{B_{ohm}} \cdot \exp\left(\frac{E_{act,ohm}}{R \cdot T}\right)$$

Butler-Volmer equation

$$j = j_{0,El} \left[\exp\left(\alpha_{El} \frac{n_e F \eta_{act,El}}{RT}\right) - \exp\left(-(1 - \alpha_{El}) \frac{n_e F \eta_{act,El}}{RT}\right) \right]$$

$$j_{0,an} = \gamma_{an} (p_{H_{2,an}})^a (p_{H_{2}O_{an}})^b \exp\left(-\frac{E_{act,an}}{RT}\right)$$

$$j_{0,cat} = \gamma_{cat} (p_{O_{2,cat}})^m \exp\left(-\frac{E_{act,cat}}{RT}\right)$$

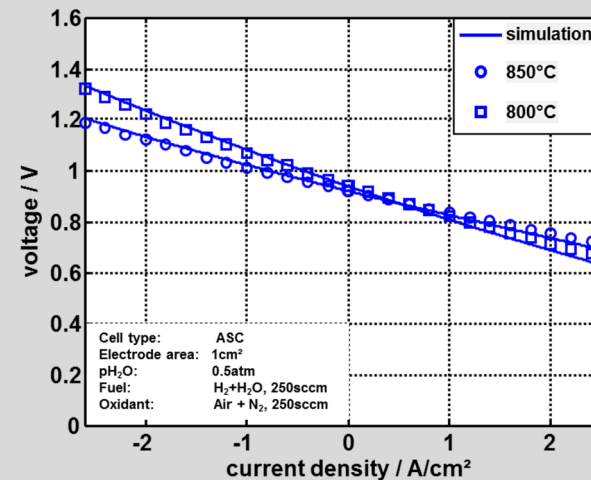
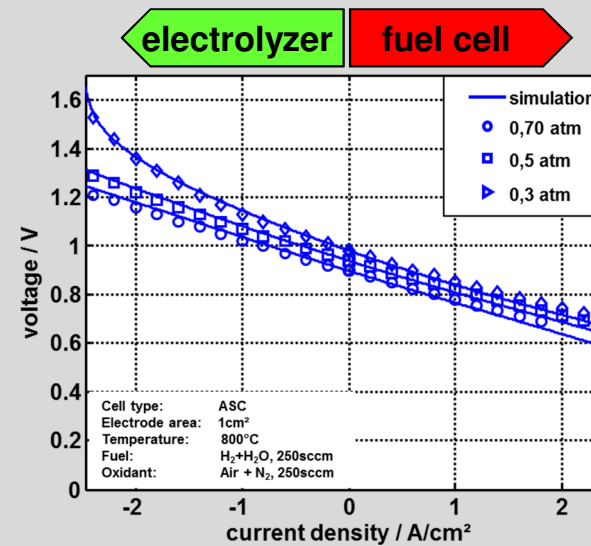
Fick's law inserted + Nernst equation with $D_i^{eff} = \psi_{el} \cdot D_i$

$$\text{Cell voltage } U_{cell}(j) = U_{OCV} - (\eta_{ohm}(j) + \eta_{conc,an}(j) + \eta_{conc,cat}(j) + \eta_{act,an}(j) + \eta_{act,cat}(j))$$

durability model ?

model parameters $p_i = f(\text{time, operating conditions})$

model validation



excellent agreement

- different temperatures
- different gases
- fuel cell and electrolyzer mode

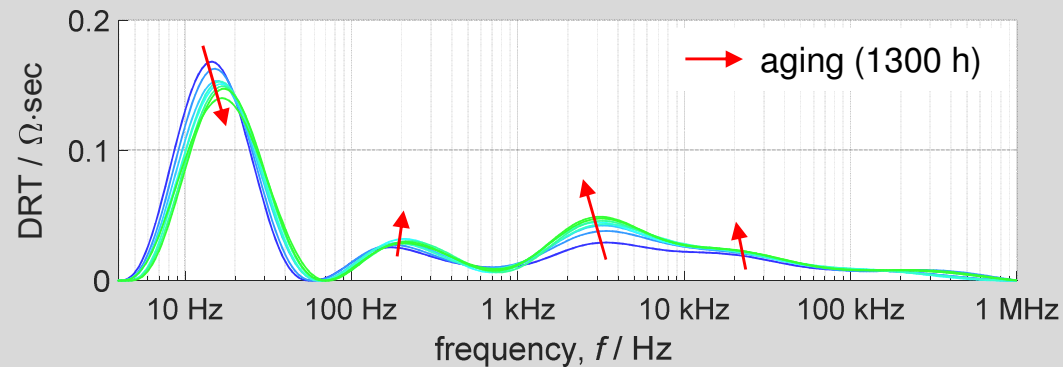
A. Leonide et al, ECS Trans. **28** (11), 341 (2010)

J.-C. Njodzefon et al., J. Electrochem. Soc., **160** (4), p. F313 (2013)

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Modelling III

Single Cell Durability Model

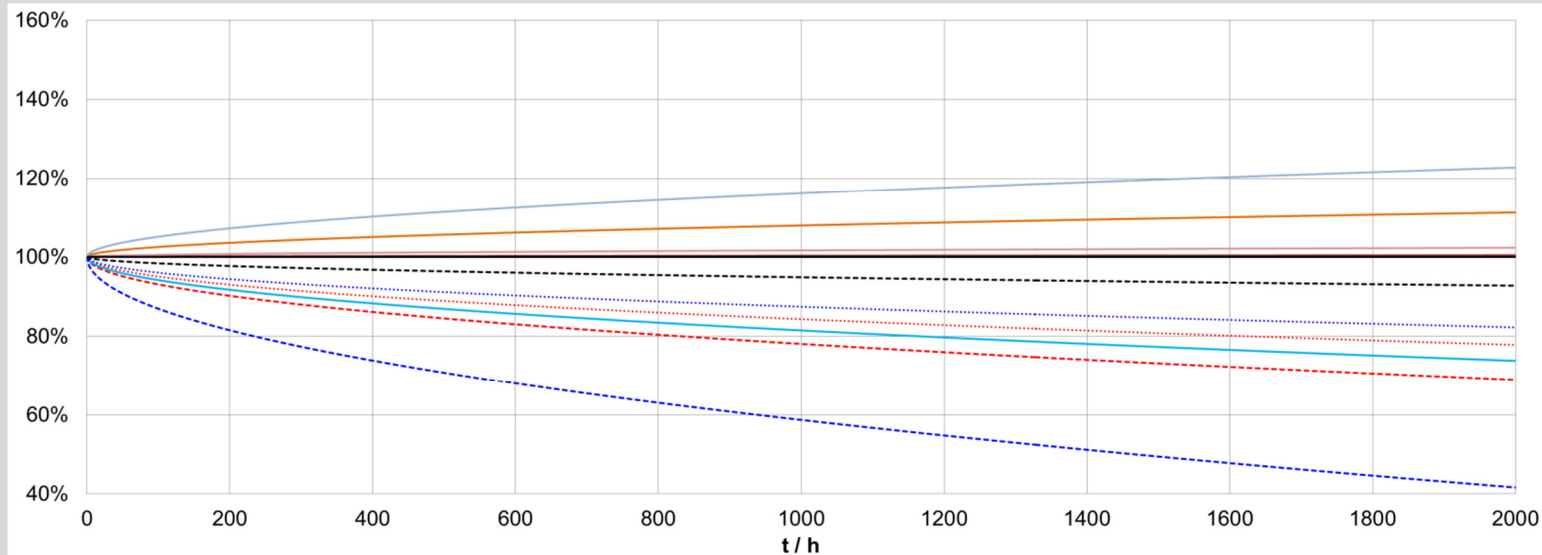


test matrix (varied parameters)

- temperature
- current density
- fuel composition
- oxidant composition
- ... to be extended

test duration: 1300 h (> 4000 h)

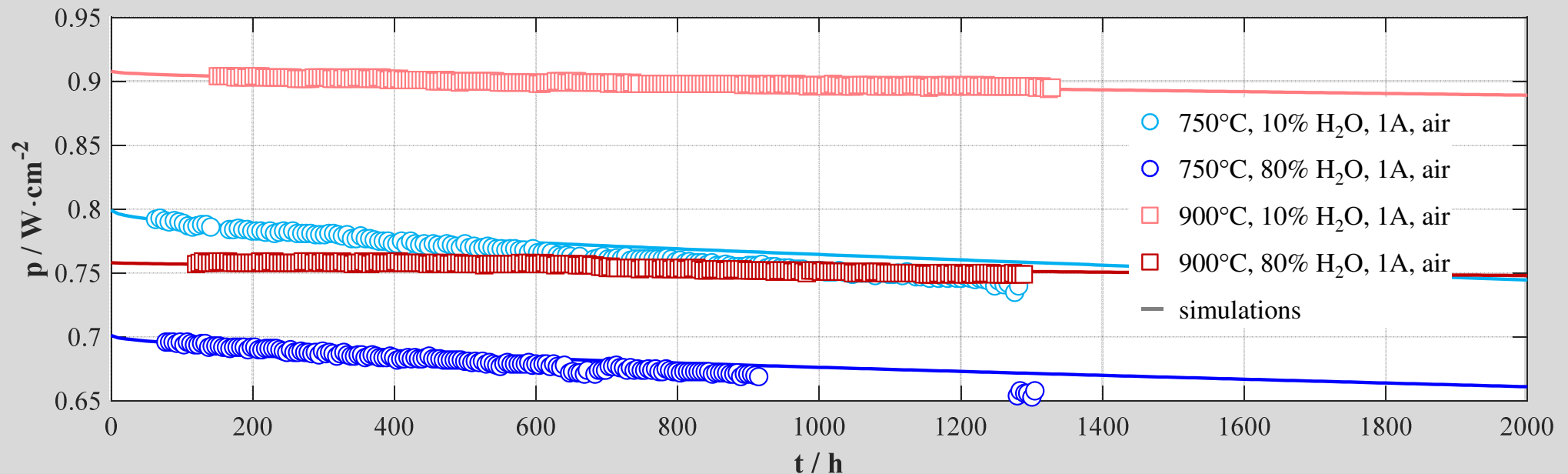
time dependency of model parameters $\rightarrow \sqrt{t}$



operating point
 $T = 900\text{ }^{\circ}\text{C}$
 $10\% \text{ H}_2 / 90\% \text{ H}_2\text{O}$
 0 A/cm^2

Single Cell Durability Model Validation

measured and simulated cell degradation

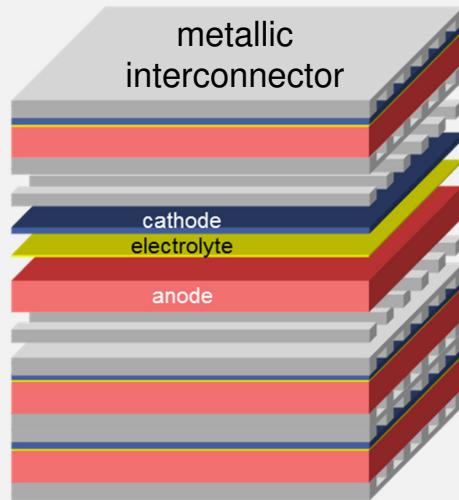


- simulations in good agreement with the measurements
- error < 2.5 mW·cm²

SOFC Stacks

Spatial Gradients → Localized Degradation

planar SOC stack

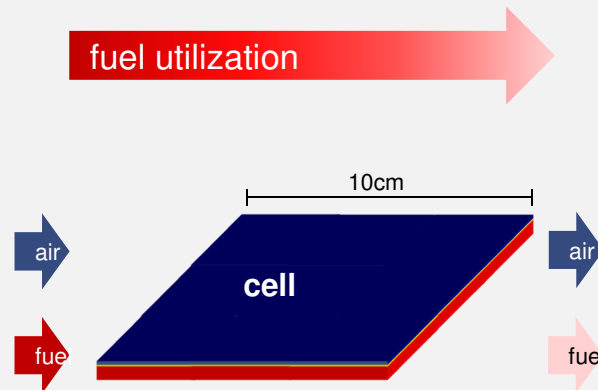


- in plane conduction
- gas conversion
- heat generation
- heat dissipation



spatial gradients

spatial gradients



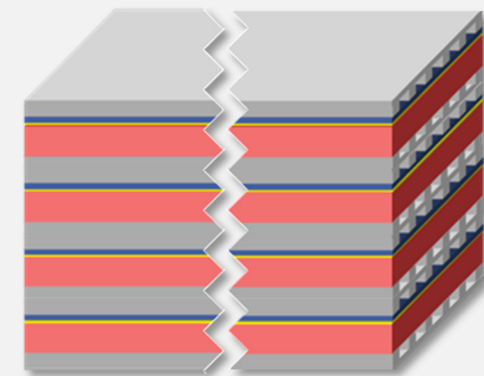
fuel utilization

temperature

electromotive force

current density

degradation model



local operating conditions



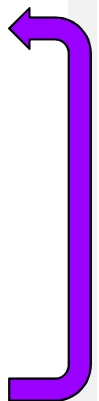
local degradation



temporal change of
local cell parameters

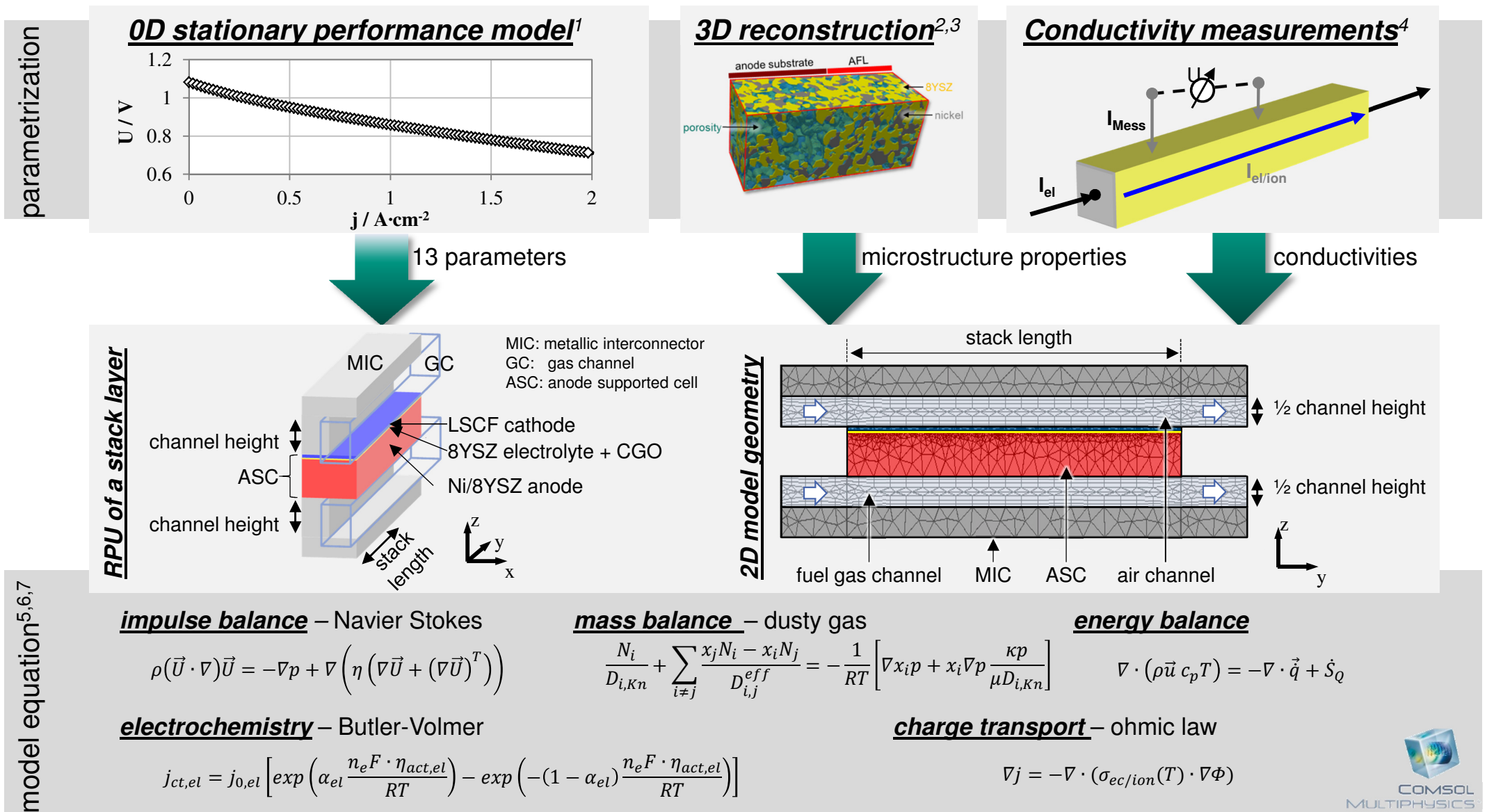


temporal change of
local operating conditions



Modelling IV

FEM Repeat Unit Model → space-resolved Performance

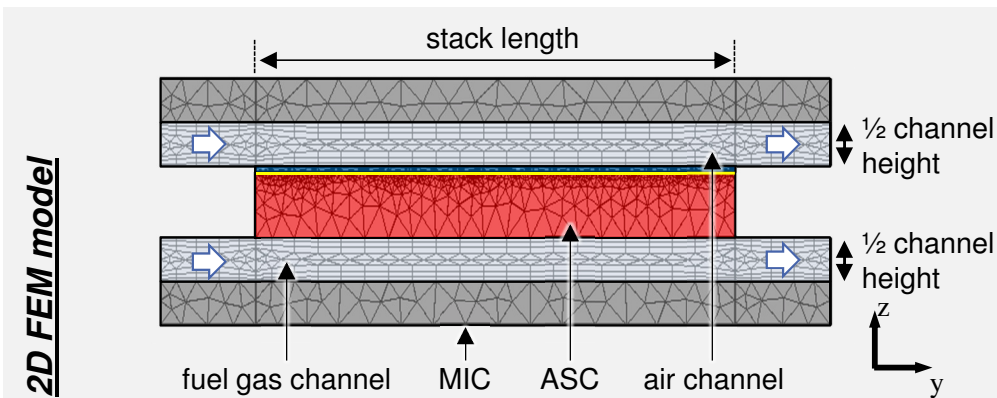


[1] A. Leonide, et. al., *J. Power Sources*, **196**, p. 7343, (2011).
[2] J. Joos, et. al., *J. Power Sources* **196**, pp. 7302-7307 (2011).
[3] J. Joos, et. al., *J. Power Sources* **246**, pp. 819-830 (2014).
[4] M. Kornely, et. al., *J. Power Sources* **196**, pp. 7209-7216 (2011).

[5] H. Geisler, et. al., *J. Electrochem. Soc.*, **161** (6), p. F778-F788 (2014).
[6] H. Geisler, et. al., *ECS Transaction*, **68** (1), p. 2151-2158 (2015).
[7] N. Russner, et. al., *ECS Transaction*, **78** (1), p. 2673-2682 (2017).

Modelling V

Stack Durability Model

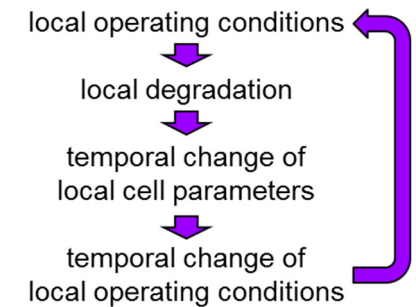


geometry

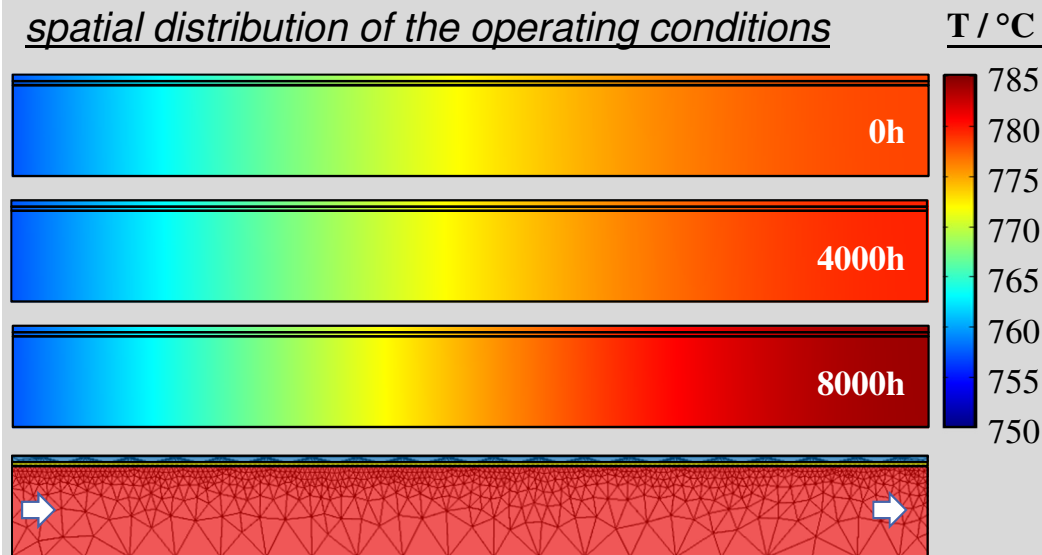
- stack width: 129mm
- stack length: 65mm
- channel height: 0.34mm

operation conditions (co-flow)

- 0.3 A/cm² (f.u. 36%)
- fuel: H₂/N₂ (50/50) + 3% H₂O, 1l/m
- oxidant: air (21% O₂), 2l/min
- temperature: 750°C



spatial distribution of the operating conditions



➤ **T_{max} and T-gradient increases**

Modelling V

Stack Durability Model

